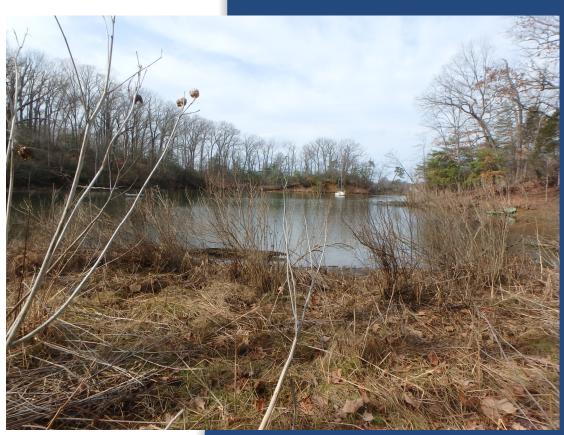
Harness Creek Gully Repair P584605

30% Schematic Design Report

Anne Arundel County, Maryland







### **TABLE OF CONTENTS**

1.0	I	NTRODUCTION	1
	1.1	Background	1
	1.2	Project Objectives	3
2.0	E	XISTING SITE CONDITIONS	3
,	2.1	Project Site Description	3
,	2.2	Federal Emergency Management Agency Regulated Floodplain	3
,	2.3	Natural Resource Inventory	3
,	2.4	Hydrologic Investigation	4
3.0	P	ROPOSED SCHEMATIC DESIGN	5
í	3.1	Design Objectives	5
•	3.2	Design Approach	5
4.0	A	DDITIONAL DESIGN CONSIDERATIONS	7
4	4.1	Natural Resource Impacts	7
	4.2	<b>Existing Utilities</b>	7
	4.3	Pedestrian and Park-Use Impacts	7
4	4.4	Stormwater BMP Data Tracking Table	7
4	4.5	Anticipated Construction Cost	7
5.0	S	UMMARY	7
6.0	R	EFERENCES	8
FIG <sup>1</sup>		S: nject Location Map	2
TAE	BLES	S:	
Tabl	e 1:	Drainage Area Hydrologic Data	
		Modeled Rainfall Events	
		Existing Discharges (cfs)	
		Riffle 100-Year Storm Event Design Values	
		Summary of Protocol 5 Impervious Acres Treatment and Length Restored	
		Proposed Annual Pollutant Load Reductions	
		Proposed Annual Pollutant Load Reductions and Impervious Area (IA) Credit	
		: Harness Creek SPSC Construction Summary	

#### APPENDICES:

- A FEMA Flood Insurance Rate Map B Natural Resources Inventory
- C Existing Hydrologic Analysis
- D Design Computations
- E Stormwater BMP Data Tracking Table F Preliminary Cost Estimate

#### 1.0 INTRODUCTION

#### 1.1 Background

The Anne Arundel County Department of Public Works investigated the Harness Creek area within Quiet Waters Park with the goal of constructing a boardwalk down to the water, storage bins, small vessel rack, and an aluminum pier for water access to the creek. A schematic design was prepared, and it was determined that the project would not move forward.

As part of this investigation, it was determined that drainage from the roadway and the upper trail, passing through a corrugated metal pipe (CMP) culvert and into the wooded area adjacent to the proposed boardwalk, was causing erosion and a gully was forming. This gully extends from the CMP culvert downstream about 450 feet before the slope flattens just upstream of the tidal interface. The gully depth ranges up to about five feet, and several large trees have fallen along the limits of the gully. The location of the Harness Creek Gully Repair is shown in Figure 1 below.

Modification opportunities for stabilization of the channel and water quality treatment were identified. As part of this effort survey and natural resource data were reviewed and collected, hydrologic computations were developed to assess existing conditions, and a field inspection was performed.

The following sections of this report include detailed descriptions of existing conditions and the schematic design developed for the gully repair. Design computations were conducted per County SPSC and Maryland Department of the Environment (MDE) stormwater facility design standards.



#### 1.2 Project Objectives

This Schematic Design Report was developed to address key project objectives as outlined below:

Complete hydrologic/hydraulic analyses of the existing system(s) to determine a design approach that restores the eroded channel to stable conditions.

Develop a design to provide maximum water quality benefits in the facility.

Document credit towards Anne Arundel County's National Pollutant Discharge Elimination System (NPDES) municipal separate storm sewer system (MS4) permit watershed restoration requirement and assisting in meeting Anne Arundel County's waste load allocation towards the Chesapeake Bay Total Maximum Daily Load (TMDL).

Detailed analyses of the watershed and site area were performed and design requirements were identified based on the results of the study. This Schematic Design Report documents each of the studies performed and documents the proposed restoration.

#### 2.0 EXISTING SITE CONDITIONS

#### 2.1 Project Site Description

Harness Creek is located in Quiet Waters Park in Annapolis, MD. A site conditions map showing existing conditions and the storm drain systems is provided in Appendix B. An eroded channel conveys storm flow from the adjacent trail, open green space, roadway, and wooded area of the park into Harness Creek through a 24" CMP pipe. The channel begins at the edge of Quiet Waters Park Rd at the outfall of a 24-inch reinforced concrete pipe (RCP), passes beneath a walking trail (24-CMP), and approximately 450ft east to Harness Creek. The main channel has an approximate 4-foot head cut and 3-foot-high banks.

Drainage to the channel originates from wooded and recreational fields. Roadway and parking areas also contribute drainage. Additionally, a section of the adjacent walking trail drains to the channel through sheet flow. The existing culverts and storm drains are in fair condition but currently clogged with debris.

#### 2.2 Federal Emergency Management Agency Regulated Floodplain

The project site is included on one Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM), Panel Identification Number 24003C0242F (Appendix A) (FEMA, October 2012). The proposed facility is not located within a special flood hazard area. It is not anticipated that the proposed project will increase flood elevations in downstream areas since the goal of the project is to detain stormwater.

#### 2.3 Natural Resource Inventory

KCI visited the site in March 2022 to perform an update of the wetland delineation that was performed originally as part of the boardwalk project. The field reconnaissance was performed for the entire study area to verify the presence or absence of wetland areas. KCI reviewed the wetland datasheets prepared previously and verified these using the *Corps of Engineers Wetland Delineation Manual*. See Appendix B for details on the wetland delineation.

Wetlands were identified near the downstream limits of the project. The channel was identified as ephemeral.

#### 2.4 Hydrologic Investigation

#### Hydrologic Parameters

Drainage Area - The drainage area of Harness Creek was delineated using the County's GIS topography (1:2400) and field verified. The area was evaluated for existing drainage conditions. Future land use changes for the drainage area were assessed using zoning GIS data provided by the County. The land use data indicated the area is projected to remain zoned as designated Parks and Open Space.

Hydrologic Soil Groups - The hydrologic soils within the drainage area were identified from the online NRCS Soil Data Mart, (Natural Resources Conservation Service, United States Department of Agriculture, January 2016). The soils within the drainage area to Harness Creek Gully Repair are primarily hydrologic soil groups (HSG) B and C soils with some A and D soils. Soils are illustrated on the drainage area maps in Appendix C.

Runoff Curve Number - The overall existing land use within the Harness Creek Gully Repair watershed are primarily parks and open space. 1.45 acres of impervious surface within the park used for parking and walking trails.

The land use information along with the drainage area were used to create NRCS Technical Release 55 (TR-55) models (Natural Resources Conservation Service, United States Department of Agriculture, June 1986) for existing and ultimate conditions. The TR-55 model uses hydrologic soil groups which characterize the runoff potential of the soil, and land use data to determine a Runoff Curve Number (RCN), which represents the runoff potential of an area. The RCN used for the existing conditions model is based on current land use. A model representing ultimate conditions was also created based on future changes in land use predicted by zoning classifications as discussed above. To approximate the RCN in the model, industrial land use was used for the institutional since industrial has the most similar impervious cover percentage to the actual impervious coverage. The subsequent curve numbers represent an impervious coverage slightly higher than the actual conditions, resulting in a conservative model. TR-55 reports are included in Appendix C and results are shown in Table 1.

Times of Concentration - The time of concentration (Tc) is the time required for runoff to travel from the most hydrologically remote point to the bottom of the drainage area. The Tc path was delineated for the drainage area using the County's aerial topography (1:2400 feet). The Tc is given in Table 1 and calculations are provided in Appendix C.

Table 1: Drainage Area Hydrologic Data

	DA (acres)	Existing RCN	Ultimate RCN	Tc (hours)
Harness Creek Gully Repair	12.92	75	75	0.22

#### Hydrologic Method

The NRCS Technical Release 20 (TR-20) method was used to estimate peak discharges reaching the Harness channel for existing and proposed conditions (NRCS-USDA, 2015). NOAA Atlas 14 rainfall depths with the Type C rainfall distribution over a 24-hour duration were used to estimate peak discharges for existing and ultimate conditions (Natural Resources Conversation Service, United States Department of Agriculture, 1992). This method uses a synthetic hydrograph based on a dimensionless unit hydrograph and rainfall depths for accepted storm events. The TR-20 inputs include the: drainage area, runoff curve number, time of concentration, and rainfall depth. Table 2 lists the design rainfall events simulated.

**Table 2: Modeled Rainfall Events** 

		Storm Event						
	1-yr	2-yr	10-yr	100-yr				
Duration (hr)	24	24	24	24				
Rainfall (in)	2.66	3.22	5.01	8.64				

#### **Hydrologic Results**

The peak discharges were estimated for 1-, 2-, 10-, and 100-year storm events for existing watershed conditions. The 100-year storm event was modeled using ultimate watershed conditions however there are no projected changes to land use within the drainage area. Table 3 lists the hydrologic results. The TR-20 model is included in Appendix C.

**Table 3: Existing Discharges (cfs)** 

	Storm Event					
Location	1-yr	2-yr	10-yr	100-yr		
Harness Creek Gully Repair Existing	9.3	14.3	32.7	74.1		

#### 3.0 PROPOSED SCHEMATIC DESIGN

#### 3.1 Design Objectives

The design approach focused on restoring the stability of the incised channel and providing water quality benefits for the watershed while attempting to increase stormwater attenuation and reduce flow velocities throughout the project limits. To accomplish these goals, the design proposes modifying the stormwater management pond by installing a Step Pool Storm Conveyance (SPSC) System from the 24" CMP inflow pipe to the outfall at harness creek. The pools contained within the SPSC will attenuate storm flows, and the underlying sand/woodchip filter will provide water quality treatment.

#### 3.2 Design Approach

The proposed SPSC along the channel consists of 12 riffle weirs, one short cascade (two-foot vertical drop), and 14 pools between the upstream 24" CMP inflow and the project outfall into Harness Creek. The riffle weirs and cascades will be constructed of cobbles and boulders with berms connecting the weirs to the stream banks, constructed of fill material. The weir structures are designed to safely convey the 100-year storm runoff of 74.1 cfs (Table 4) as it transitions down 14 feet over a length of approximately 450 feet. All proposed grading surrounding pools and weir structures is at a 3:1 slope. All structures follow the NRCS-MD 378 small pond restriction and have embankments of less than four feet.

**Table 4: Riffle 100-Year Storm Event Design Values** 

Weir Top Width (ft)	Weir Length (ft)	Weir Depth (ft)	Cobble Mean Diameter (d50) (in.)	100- YR Q (cfs)	Full- Flow Capacity Q (cfs)	Full- Flow Velocity (fps)	Maximum Allowable Velocity (fps)
16	8	.92	9	74.1	74.2	7.6	7.7

#### Restoration Credit and Nutrient Reduction Analysis

The proposed Harness Creek Gully restoration is dry step pool storm conveyance system (SPSC) within an incised ephermal channel at the outfall of corrugated metal pipe. SPSCs, or dry Regenerative Storm Conveyances (RSC), are eligible for credit and nutrient reductions for Protocol 4 (Dry Channel RSC as an Upland Stormwater Retrofit) and Protocol 5 (Outfall and Gully Stabilization (OGS) Practices), based on *Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed* (Urban Stormwater Workgroup, 2019).

#### Protocol 4

Protocol 4 computes an annual nutrient and sediment reduction rate for the contributing drainage area to a qualifying dry channel RSC project. The modifications provide 7,758 cubic feet of water quality treatment, treating 109.56% of the target volume for treatment of the upstream drainage area. This water quality volume is based on volume stored within the SPSC pools. Table 6 below shows summary of treatment needed for the upstream drainage area versus proposed water quality treatment.

Table 6: Summary of Required vs. Proposed Water Quality Treatment

	WQv (ac-ft)	Equivalent Rainfall Depth Treated (inches)	Impervious Area Treated (acres)
Required	0.16	1.00	
Proposed	0.18	1.10	1.45

#### Protocol 5

Protocol 5 is an adaptation of the prevented sediment protocol that is applied to highly incised channels in the headwater transition zone that experience severe vertical erosion problems. Protocol 5 was calculated by determining the difference between existing conditions and interpolating an estimated equilibrium channel geometry using bulk density, grain size distribution, cross sectional data from channel the existing channel, and an estimate equilibrium bank slope. Table 7 below shows summary of the equivalent impervious treatment acres restored (EIA<sub>f</sub>), length restored, and impervious acres credit per linear foot restored.

Table 7: Summary of Protocol 5 Impervious Acres Treatment and Length Restored

Impervious Treatment Acres Restored (ac)	Length Restored (LF)	Impervious Acres credit per Linear Foot Restored (ac/LF)
22.53	457	0.05

A summary of the reduced annual pollutant loads per acre per year for the two protocols for the proposed retrofit at Harness Creek Gully can be found in Table 8 below.

**Table 8: Proposed Annual Pollutant Load Reductions** 

_	TN (lbs)	TP (lbs)	TSS (tons)
Protocol 4	6.88	1.49	3,094
Protocol 5 (over 30 years)	182.23	83.92	159,849
Total	189.11	85.41	162,943

The treatment provided using Protocol 4, as an equivalent impervious area treated, is approximately 1.45 acres. The prevented sediment associated with the stabilization of the gully, as calculated using Protocol 5, generates an equivalent impervious area treated of approximately 22.53 acres. Combined, this produced a credit for the project of 23.98 acres of treatment impervious area. All computations for the schematic design of the modifications to Harness Creek can be found in Appendix D.

#### 4.0 ADDITIONAL DESIGN CONSIDERATIONS

#### 4.1 Natural Resource Impacts

The proposed SPSC system will impact several large trees along the tributary corridor. These trees, along with several others, will be removed. Wetlands present in the tidal zone will be temporarily impacted.

#### 4.2 Existing Utilities

No utilities were identified within the proposed project limits.

#### 4.3 Pedestrian and Park-Use Impacts

During construction, the project as proposed will include use of an existing parking area adjacent to the project. A walking trail will be used to access the stabilized construction entrance from the parking area. Staging will be provided in the parking lot. This will have an impact on park users, with parking reduction and rerouting of pedestrians around the project entrance.

#### 4.4 Stormwater BMP Data Tracking Table

In accordance with the County, the Stormwater BMP Data Tracking Table for Harness Creek Gully Repair is included in Appendix E.

#### 4.5 Anticipated Construction Cost

Appendix F contains a preliminary construction cost estimate developed for the schematic design. The proposed Harness Creek SPSC system cost, including a 30% contingency is approximately \$294,000. The cost estimate will be refined during subsequent design phases.

#### 5.0 SUMMARY

In order to meet the County's stormwater management goals and provide stabilization for an eroded gully to Harness Creek in Quiet Waters Park located in Annapolis, MD, the design proposes to install a dry SPSC system within the existing channel. The location of the existing corrugated metal inflow pipe is proposed to remain the same. The proposed conveyance system

promotes stormwater retention and water quality treatment. Tables 8 and 9 below summarize the benefits of the proposed SPSC system.

Table 9: Proposed Annual Pollutant Load Reductions and Impervious Area (IA) Credit

	TN (lbs)	TP (lbs)	TSS (tons)	IA Credit
Protocol 4	6.88	1.49	3,094	1.45
Protocol 5 (over 30 years)	182.23	83.92	159,849	22.53
Total	189.11	85.41	162,943	23.98

**Table 10: Harness Creek SPSC Construction Summary** 

	Cost	Impervious Acres Treated	Cost per Impervious Acre Treated
Proposed SPSC	\$293,886	23.98	\$12,255

#### 6.0 REFERENCES

Anne Arundel County. Online GIS Data. Anne Arundel County, Annapolis, Maryland.

Anne Arundel County. "Stormwater Management Practices and Procedures Manual". 2012. Anne Arundel County, Annapolis, Maryland.

Anne Arundel County. "Regenerative Step Pool Storm Conveyance (SPSC) – Design Guidelines". 2021. Anne Arundel County, Annapolis, Maryland.

Federal Emergency Management Agency. Flood Insurance Rate Map Number 24003C0033E. Effective Date October 2012.

Maryland Department of the Environment. "Maryland Stormwater Design Manual Volume I & II". 2009. Baltimore, MD.

Maryland Department of the Environment. "Accounting for Stormwater Wasteload Allocations and Impervious Acres Treated". June 2020. Baltimore, Maryland.

Natural Resources Conversation Service, United States Department of Agriculture. "Urban Hydrology for Small Watersheds". Technical Release Number 55. June 1986.

Natural Resources Conversation Service, United States Department of Agriculture. "Computer Program for Project Formulation Hydrology". WinTR-20, Version 3.20. March 2015.

Natural Resources Conversation Service, United States Department of Agriculture. "NRCS-MD Code No.378 Pond Standards/Specifications". January, 2000.

Natural Resources Conversation Service, United States Department of Agriculture. Web Soil Survey. Accessed March 2022.

Urban Stormwater Work Group (Stream Restoration Group 2). 2019. "Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed". Chesapeake Bay Foundation.

Urban Stormwater Work Group (Stream Restoration Group 2). 2019. "Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed". Chesapeake Bay Foundation.

# **Appendix A – FEMA Flood Insurance Rate Map**

### NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations tables in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations tables should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was Universal Transverse Mercator (UTM) zone 18N. The **horizontal datum** was NAD 83, GRS 80 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of information shown on this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <a href="http://www.ngs.noaa.gov">http://www.ngs.noaa.gov</a> or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282

(301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <a href="http://www.ngs.noaa.gov">http://www.ngs.noaa.gov</a>.

Base map information was provided by the Anne Arundel County GIS Department. The digital ortho imagery was compiled by Axis Geospatial at a scale of 1:100 with a 6 inch ground pixel resolution, and published by the Maryland Department of Information Technology in 2011.

This map reflects more detailed and up-to-date **stream channel configurations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to confirm to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

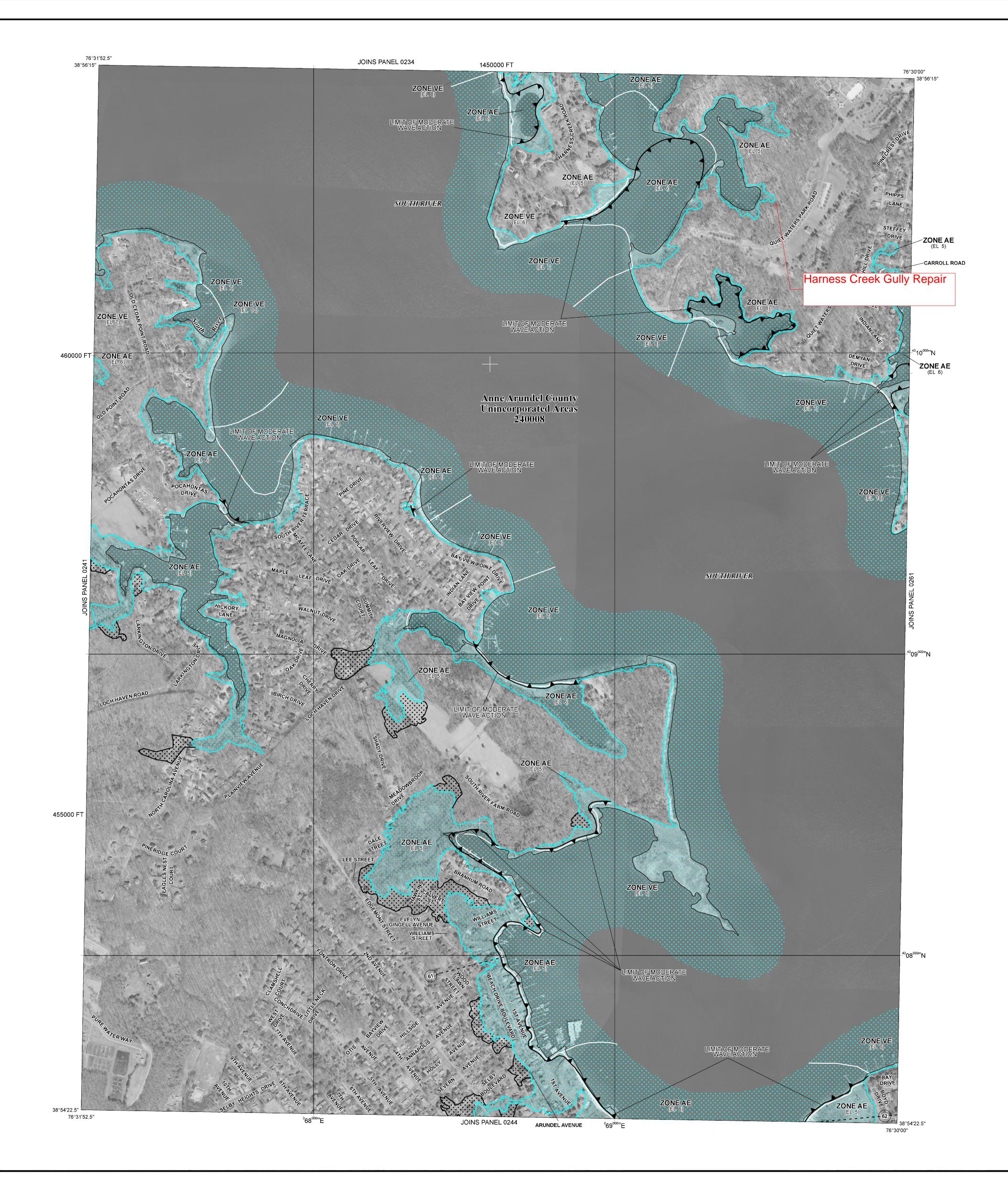
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

The AE Zone category has been divided by a **Limit of Moderate Wave Action** (**LiMWA**). The LiMWA represents the approximate landward limit of the 1.5-foot breaking wave. The effects of wave hazards between the VE Zone and the LiMWA (or between the shoreline and the LiMWA for areas where VE Zones are not identified) will be similar to, but less severe than those in the VE Zone.

Contact the **FEMA Map Information eXchange** at 1-877-336-2627 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Information eXchange may also be reached by Fax at 1-800-358-9620 and their website at <a href="http://www.msc.fema.gov/">http://www.msc.fema.gov/</a>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <a href="http://www.fema.gov/business/nfip">http://www.fema.gov/business/nfip</a>.



## LEGEND

SPECIAL FLOOD HAZARD AREAS SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface

No Base Flood Elevations determined.

ZONE AE Base Flood Elevations determined.

elevation of the 1% annual chance flood.

ZONE V

ZONE X

ZONE D

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also

ZONE AR

Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide

protection from the 1% annual chance or greater flood.

ZONE A99

Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); no Base Flood

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with

Elevations determined.

NE VE Coastal flood zone with velocity hazard (wave action); Base Flood

Elevations determined.

FLOODWAY AREAS IN ZONE AE

The flood way is the channel of a stream plus any adjacent flood plain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases

in flood heights.

OTHER FLOOD AREAS

average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

Areas determined to be outside the 0.2% annual chance floodplain.

Areas in which flood hazards are undetermined, but possible.

OTHERWISE PROTECTED AREAS (OPAs)

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

1% annual chance floodplain boundary0.2% annual chance floodplain boundary

0.2% annual chance floodplain bour
 Floodway boundary

\_\_\_\_ Zone D boundary

CBRS and OPA boundary

Boundary dividing Special Flood Hazard Area Zones and

boundary dividing Special Flood Hazard Areas of different
Base Flood Elevations, flood depths or flood velocities.

Limit of Moderate Wave Action

Base Flood Elevation line and value; elevation in feet\*

(EL 987) Base Flood Elevation value where uniform within zone; elevation in feet\*

\* Referenced to the North American Vertical Datum of 1988

(A) Cross section line

M1.5

Transect line

Transect line

87°07'45", 32°22'30"

Geographic coordinates referenced to the North American

Datum of 1983 (NAD 83), Western Hemisphere

<sup>24</sup>**76**<sup>000m</sup>N 1000-meter Universal Transverse Mercator grid values, zone 18N

600000 FT 5000-foot grid values: Maryland State Plane coordinate system (FIPSZONE 1900), Lambert Conformal Conic projection

DX5510 x

Bench mark (see explanation in Notes to Users section of this FIRM panel)

River Mile

MAP REPOSITORY Refer to listing of Map Repositories on Map Index

EFFECTIVE DATE OF COUNTYWIDE

FLOOD INSURANCE RATE MAP October 16, 2012

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL February 18, 2015 - To incorporate new detailed coastal flood hazard analysis and to reflect updated topographic information.

For community, many variation history, prior to country unido manning, vefor to the Community

For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in this community, contact your Insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

MAP SCALE 1" = 500'
250 0 500 1000

0 150

PANEL 0242F

FIRM

FLOOD INSURANCE RATE MAP

ANNE ARUNDEL COUNTY, MARYLAND

PANEL 242 OF 385

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

AND INCORPORATED AREAS

SEE MAP INDEX FOR F

COMMUNITYNUMBERPANELSUFFIXANNE ARUNDEL COUNTY2400080242F

Notice to User: The **Map Number** shown below should be

used when placing map orders; the Community Number shown above should be used on insurance applications for the



MAP NUMBER 24003C0242F

MAP REVISED FEBRUARY 18, 2015

Federal Emergency Management Agency

# **Appendix B – Natural Resources Inventory**

April 11, 2022

Ms. Melissa Harlinski Anne Arundel County Department of Public Works 2662 Riva Road Annapolis, MD 21401

**RE:** Harness Creek

Quiet Waters Park Annapolis, MD

**SUB:** Summary of Findings Report

Dear Ms. Harlinski:

The Anne Arundel County Department of Public Works is proposing a regenerative step pool stormwater conveyance within Quiet Waters Park, at the headwaters of Harness Creek. As part of this effort, KCI Technologies, Inc. (KCI) reviewed and confirmed a previous wetland delineation performed by others. Resources throughout the study area were verified using criteria established in the Corps of Engineers Wetlands Delineation Manual (Environmental Laboratory, 1987), the Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Atlantic and Gulf Coastal Plain (Version 2.0) (Environmental Laboratory, 2010), and subsequent guidance documents. Additionally, KCI confirmed a tree survey performed by others.

The project area consists of forested parkland adjacent to tidal waters. A nontidal wetland borders the tidal waters at the western edge of the study area. An ephemeral channel flows west through the study area, loses definition to become overflow, and flow eventually enters the nontidal and tidal wetlands.

#### Wetland Methodology

A field reconnaissance was performed for the entire study area to verify the presence or absence of wetland areas during March 2022. KCI reviewed wetland datasheets previously prepared by others and compared the data to conditions onsite. Wetlands were verified using the criteria outlined in the *Corps of Engineers Wetlands Delineation Manual* (Environmental Laboratory, 1987) and the *Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Atlantic and Gulf Coastal Plain Region (Version 2.0)* (Environmental Laboratory, 2010). An

Employee-Owned Since 1988

Existing Conditions Map prepared by KCI is included in Appendix A to this report. Wetland datasheets are included in Appendix B.

#### **Findings**

The field investigation performed during March 2022 located one nontidal wetland system and one tidal wetland system. An ephemeral channel was also identified within the study area.

#### Wetlands

Wetland DP-1 is a palustrine, forested, broad-leaved deciduous, seasonally flooded/saturated (PFO1E) wetland dominated by black gum (Nyssa sylvatica), sweet gum (Liquidambar styraciflua), American elm (Ulmus americana), American sycamore (Platanus occidentalis), blackhaw viburnum (Viburnum prunifolium), jewelweed (Impatiens capensis), Japanese stiltgrass (Microstegium vimineum), and Jack in the Pulpit (Arisaema triphyllum). Groundwater contributes hydrology to the wetland and hydric soils were identified.

The tidal fringe wetland along Harness Creek is dominated by eastern baccharis (Baccharis halimfolia), cattail (Typha latifolia), and sea-side club rush (Schoenoplectus robustus). The wetland is tidally influenced.

#### Waterways

An ephemeral channel originates within a forested area, approximately 400 feet east of Harness Creek. The channel conveys overland flow east, loses definition, and this flow eventually enters the wetland along the edge of Harness Creek.

#### Tree Survey

KCI walked the study area to verify a tree survey performed by others. KCI verified species, size, and condition of more than 200 trees located in the study area. Species ranged from sweet gum to tulip poplar (Liriodendron tulipifera), American sycamore, red maple (Acer rubrum), box elder (Acer negundo), and sassafras (Sassafras albidum). A number of trees were noted to be dead. An existing conditions plan prepared by others illustrating the trees and KCI's updated tree survey data are included as Appendix C to this report.

RISE TO THE CHALLENGE

WWW.KCI.COM

If you should have any questions regarding the information outlined above, or if you require additional information concerning this memorandum, please do not hesitate to contact me.

Very truly yours,

KCI TECHNOLOGIES, INC.

Junifu ABiel

Jennifer Bird

Senior Project Manager Natural Resources Practice Direct Dial Phone: 410.316.7959

Email: jennifer.bird@kci.com

**Enclosures:** Appendix A: Existing Conditions Map, prepared by KCI

Appendix B: Wetland Datasheets

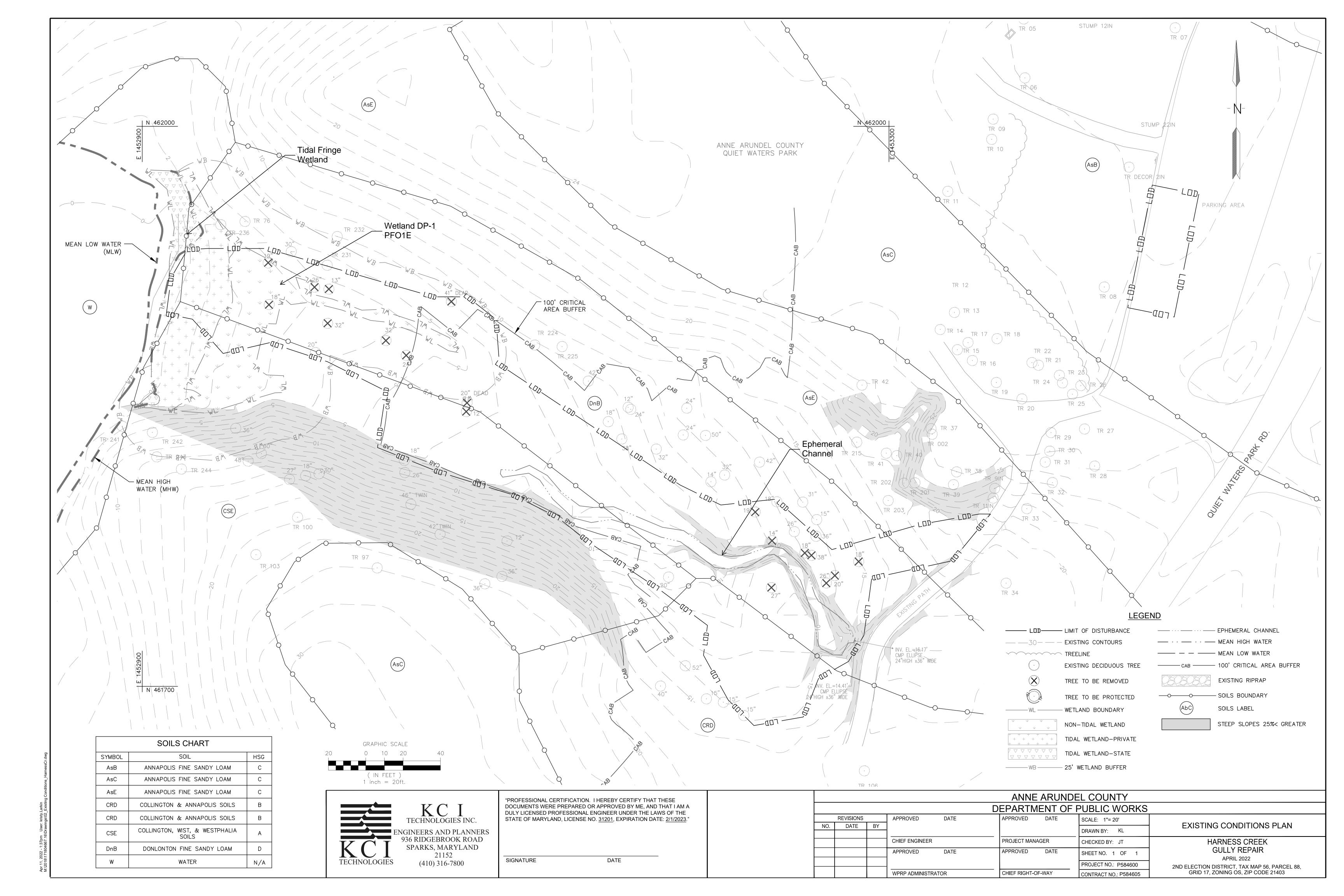
Appendix C: Tree Survey Map and Inventory

WWW.KCI.COM

RISE TO THE CHALLENGE

## **APPENDIX A**

Existing Conditions Map



## **APPENDIX B**

Wetland Datasheets

### WETLAND DETERMINATION DATA FORM – Atlantic and Gulf Coastal Plain Region

Project/Site:	City/Co	unty:		Sampling Date:
Applicant/Owner:			State:	Sampling Point:
Investigator(s):	Section	, Township, Range:		
Are Vegetation, Soil, or Hydr	ology naturally problemati	ic? (If needed, o	explain any answers	s in Remarks.)
SUMMARY OF FINDINGS – Attac	h site map showing samp	oling point location	ons, transects,	important features, et
Hydrophytic Vegetation Present?	'es No			
	es No		V	M-
		within a Wetland?	Yes	No
Remarks:				
HADBOLOGA				
			Secondary Indicat	ore (minimum of two required)
· •	uired: check all that apply)		-	
				, ,
· · ·		U)		
			=	
Water Marks (B1)				
Sediment Deposits (B2)				
Drift Deposits (B3)	Recent Iron Reduction in T	illed Soils (C6)	Saturation Vis	sible on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Thin Muck Surface (C7)			
		)		
	37)			
			Spnagnum mo	OSS (D8) (LRR I, U)
	No Denth (inches):			
			Hydrology Present	? Yes No
(includes capillary fringe)				100 110
Describe Recorded Data (stream gauge, m	onitoring well, aerial photos, previ	ious inspections), if ava	ailable:	
Remarks:				
Landform (hillslope, terrace, etc.):				
Are Vegetation Soil or Hydrology significantly disturbed? Are "Normal Circumstances" present? Yes No Are Vegetation Soil or Hydrology naturally problematic? (If needed, explain any answers in Remarks.)  SUMMARY OF FINDINGS — Attach site map showing sampling point locations, transects, important features, etc.  Hydrophytic Vegetation Present? Yes No Weltand Hydrology Present? Yes No Soil Present? Yes No Depth (inches): Water Mark Present? Yes No Depth (inches): Water Table Present? Yes No Depth (inches): Water Soil Prese				

e Stratum (Plot size:)			Indicator	Dominance Test w	orksheet:		
	70 COVE		Status				
							(4)
	Total Number of Dominant Species Across All Strata:  Percent of Dominant Species Across All Strata:  Percent of Dominant Species That Are OBL, FACW, or I  Prevalence Index worksI  Total % Cover of.  OBL species  FACW species  FACW species  FACU species  FACU species  FACU species  Column Totals:  Prevalence Index = Hydrophytic Vegetation  1 - Rapid Test for Hyd  2 - Dominance Test is  3 - Prevalence Index is  Problematic Hydrophy  Problematic Hydrophy  Indicators of hydric soil and be present, unless disturb  Definitions of Four Vege  Tree — Woody plants, excluding in Definition of Size, and woody plants  Sapling/Shrub — Woody plants is distarb.  Sapling/Shrub — Woody plants of size, and woody plants  Woody vine — All woody wheight.  — Total Cover  20% of total cover:  — Total Cover  Solve of total cover:  — Total Cover	, W, or FAC:	-	(A)			
				Total Number of Do	minant		
				Species Across All	Strata:	-	(B)
				Percent of Dominar	nt Species		
							(A/l
				Provolence Index	workshooti		
						NA. déimhe he	
50% of total cover:	20% of	total cover:					
oling/Shrub Stratum (Plot size:)				FAC species	×	(3 =	
				FACU species	×	(4 =	
				UPL species	x	< 5 =	
				Column Totals:	(/	A)	(E
				Prevalence In	dex = B/A =	·	
				Hydrophytic Vege	tation Indic	ators:	
				1 - Rapid Test	for Hydrophy	ytic Vegetatio	n
				2 - Dominance	Test is >50°	%	
				3 - Prevalence	Index is ≤3.0	0 <sup>1</sup>	
	:	= Total Cov	er	Problematic Hy	drophytic Ve	egetation¹ (Ex	(plain)
50% of total cover:	20% of	total cover:		<u> </u>	. ,	,	. ,
b Stratum (Plot size:)							gy must
				Definitions of Fou	r Vegetation	n Strata:	
				Tuna Mandu plan	ممالين المناسية	i	7.0)
					. Drodot noigi	in (DDi i), 10g	ai aiooo
				Conline/Church \A	loody planta	. ovoludina vi	naa laa
					g. oato. t. a.	. 0.20 ()	
				of size, and woody	plants less ti	nan 3.28 π tai	н.
				Woody vine – All v	voody vines	greater than	3.28 ft ir
				height.			
	:	= Total Cov	er				
50% of total cover:	20% of	total cover:					
ody Vine Stratum (Plot size:)							
	· · · · · · · · · · · · · · · · · · ·			Present?	Yes	No	
	20% of	total cover:					_

SOIL							Sampling Point:
Profile Desc	ription: (Describe	to the dep	th needed to docun	nent the indicator	or confirm	n the absence	of indicators.)
Depth	Matrix		Redox	k Features			
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u> Type <sup>1</sup>	<u>Loc<sup>2</sup></u>	Texture	Remarks

Depth	Matrix		Redo	x Features			
(inches)	Color (moist)	%	Color (moist)	%Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
							_
				- <del> </del>	<del>_</del>		
		<del></del>					
	ncentration, D=Deple				Grains.		=Pore Lining, M=Matrix.
Hydric Soil I	ndicators: (Applica	ble to all LR	Rs, unless othe	rwise noted.)		Indicators for	Problematic Hydric Soils <sup>3</sup> :
Histosol	(A1)	_	Polyvalue Be	elow Surface (S8)	(LRR S, T, U)	1 cm Mucl	k (A9) <b>(LRR O)</b>
	ipedon (A2)		-	urface (S9) (LRR \$			k (A10) <b>(LRR S)</b>
Black His				xy Mineral (F1) <b>(LF</b>			Vertic (F18) (outside MLRA 150A,B)
<del></del>	n Sulfide (A4)	•		ed Matrix (F2)	•		Floodplain Soils (F19) (LRR P, S, T)
	Layers (A5)	•	Depleted Ma				s Bright Loamy Soils (F20)
	Bodies (A6) (LRR P,	T, U)	Redox Dark			(MLRA	
	cky Mineral (A7) <b>(LRF</b>			rk Surface (F7)			nt Material (TF2)
	esence (A8) (LRR U)	, -, <b>-,</b>	Redox Depre				low Dark Surface (TF12)
<del></del>	ck (A9) (LRR P, T)	•	Nedox Bepit Marl (F10) <b>(I</b>				plain in Remarks)
<del></del>	Below Dark Surface	(A11)		hric (F11) (MLRA	151)	Other (EX	olain in remarks)
	rk Surface (A12)	(/ ( ) / )		nese Masses (F12)		7) <sup>3</sup> Indicato	rs of hydrophytic vegetation and
	airie Redox (A16) <b>(M</b> I	ΡΔ 150Δ)		ace (F13) <b>(LRR P</b> ,			d hydrology must be present,
	ucky Mineral (S1) <b>(LF</b>			(F17) <b>(MLRA 151</b>			disturbed or problematic.
-	leyed Matrix (S4)	(it 0, 0)		rtic (F18) <b>(MLRA</b>		unicss	distarbed or problematic.
	edox (S5)	•		oodplain Soils (F1		ιΔ)	
	Matrix (S6)			Bright Loamy Soils			30)
		T 11\	Anomalous i	Silgili Loamy Solls	(FZU) (IVILKA	1 149A, 155C, 15	(טפו
	face (S7) (LRR P, S,	1, 0)					
	ayer (if observed):						
Type:			=				
Depth (inc	:hes):		_			Hydric Soil Pre	esent? Yes No
Remarks:							

### WETLAND DETERMINATION DATA FORM – Atlantic and Gulf Coastal Plain Region

Project/Site:	City/Co	unty:		Sampling Date:
Applicant/Owner:			State:	Sampling Point:
Investigator(s):	Section	, Township, Range:		
Landform (hillslope, terrace, etc.):				
Subregion (LRR or MLRA):				
Soil Map Unit Name:				
Are climatic / hydrologic conditions on the sit				
Are Vegetation, Soil, or Hydr				
Are Vegetation, Soil, or Hydr	ology naturally problemati	ic? (If needed, o	explain any answers	s in Remarks.)
SUMMARY OF FINDINGS – Attac	h site map showing samp	oling point location	ons, transects,	important features, et
Hydrophytic Vegetation Present? Y	'es No			
	es No	Is the Sampled Area	V	M-
	'es No	within a Wetland?	Yes	No
Remarks:				
HYDROLOGY				
Wetland Hydrology Indicators:			Secondary Indicat	ors (minimum of two required)
Primary Indicators (minimum of one is requ	uired: check all that apply)		Surface Soil C	
Surface Water (A1)	Aquatic Fauna (B13)			etated Concave Surface (B8)
High Water Table (A2)	Marl Deposits (B15) (LRR	U)	Orainage Patt	
Saturation (A3)	Hydrogen Sulfide Odor (C		Moss Trim Lin	
Water Marks (B1)	Oxidized Rhizospheres ald			Vater Table (C2)
Sediment Deposits (B2)	Presence of Reduced Iron		Crayfish Burro	
Drift Deposits (B3)	Recent Iron Reduction in T	illed Soils (C6)	Saturation Vis	sible on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Thin Muck Surface (C7)		Geomorphic F	
Iron Deposits (B5)	Other (Explain in Remarks	)	Shallow Aquit	
Inundation Visible on Aerial Imagery (E	37)		FAC-Neutral	
Water-Stained Leaves (B9) Field Observations:			Spnagnum mo	oss (D8) <b>(LRR T, U)</b>
	No Depth (inches):			
	No Depth (inches):			
	No Depth (inches):		Hydrology Present	? Yes No
(includes capillary fringe)				100 110
Describe Recorded Data (stream gauge, m	onitoring well, aerial photos, previ	ious inspections), if ava	ailable:	
Remarks:				

e Stratum (Plot size:)	Absolute % Cover	Dominant	Indicator	Dominance Test w	orksheet:		
	70 COVE		Status				
				Number of Dominal			(4)
				That Are OBL, FAC	, W, or FAC:	-	(A)
				Total Number of Do	minant		
				Species Across All	Strata:	-	(B)
				Percent of Dominar	nt Species		
				That Are OBL, FAC			(A/l
				Prevalence Index	workshooti		
						NA. déimhe he	
				Total % Cover			
		= Total Cov		OBL species			
50% of total cover:	20% of	total cover:		FACW species			
oling/Shrub Stratum (Plot size:)				FAC species	×	(3 =	
,				FACU species	×	(4 =	
				UPL species	x	< 5 =	
				Column Totals:	(/	A)	(E
				Prevalence In	dex = B/A =	·	
				Hydrophytic Vege	tation Indic	ators:	
				1 - Rapid Test	for Hydrophy	ytic Vegetatio	n
				2 - Dominance	Test is >50°	%	
				3 - Prevalence	Index is ≤3.0	0 <sup>1</sup>	
	:	= Total Cov	er	Problematic Hy	drophytic Ve	egetation¹ (Ex	(plain)
50% of total cover:	20% of	total cover:		<u> </u>	. ,	,	. ,
<u>b Stratum</u> (Plot size:)				<sup>1</sup> Indicators of hydric be present, unless			gy must
				Definitions of Fou	r Vegetation	n Strata:	
				Tuna Mandu plan	م مناه در المدالية	i	7.0)
				Tree – Woody plan more in diameter at			
				height.	. Drodot noigi	in (DDi i), 10g	ai aiooo
				Conline/Church \A	loody planta	. ovoludina vi	naa laa
				Sapling/Shrub – W than 3 in. DBH and			
					g. cato. t. a.	. 0.20 ()	
				Herb – All herbace			
				of size, and woody	plants less ti	nan 3.28 π tai	н.
				Woody vine – All v	voody vines	greater than	3.28 ft ir
				height.			
	:	= Total Cov	er				
50% of total cover:	20% of	total cover:					
ody Vine Stratum (Plot size:)							
				Hydrophytic			
	· · · · · · · · · · · · · · · · · · ·	= Total Cov		Vegetation Present?	Yes	No	
	20% of	total cover:					_

SOIL							Sampling Point:
Profile Desc	ription: (Describe	to the dep	th needed to docun	nent the indicator	or confirm	n the absence	of indicators.)
Depth	Matrix		Redox	k Features			
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u> Type <sup>1</sup>	<u>Loc<sup>2</sup></u>	Texture	Remarks

Depth	Matrix		Redo	x Features			
(inches)	Color (moist)	%	Color (moist)	%Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
							_
				- <del> </del>	<del>_</del>		
		<del></del>					
	ncentration, D=Deple				Grains.		=Pore Lining, M=Matrix.
Hydric Soil I	ndicators: (Applica	ble to all LR	Rs, unless othe	rwise noted.)		Indicators for	Problematic Hydric Soils <sup>3</sup> :
Histosol	(A1)	_	Polyvalue Be	elow Surface (S8)	(LRR S, T, U)	1 cm Mucl	k (A9) <b>(LRR O)</b>
	ipedon (A2)		-	urface (S9) (LRR \$			k (A10) <b>(LRR S)</b>
Black His				xy Mineral (F1) <b>(LF</b>			Vertic (F18) (outside MLRA 150A,B)
<del></del>	n Sulfide (A4)	•		ed Matrix (F2)	•		Floodplain Soils (F19) (LRR P, S, T)
	Layers (A5)	•	Depleted Ma				s Bright Loamy Soils (F20)
	Bodies (A6) (LRR P,	T, U)	Redox Dark			(MLRA	
	cky Mineral (A7) <b>(LRF</b>			rk Surface (F7)			nt Material (TF2)
	esence (A8) (LRR U)	, -, <b>-,</b>	Redox Depre				low Dark Surface (TF12)
<del></del>	ck (A9) (LRR P, T)	•	Nedox Bepit Marl (F10) <b>(I</b>				plain in Remarks)
<del></del>	Below Dark Surface	(A11)		hric (F11) (MLRA	151)	Other (EX	olain in remarks)
	rk Surface (A12)	(/ ( ) / )		nese Masses (F12)		7) <sup>3</sup> Indicato	rs of hydrophytic vegetation and
	airie Redox (A16) <b>(M</b> I	ΡΔ 150Δ)		ace (F13) <b>(LRR P</b> ,			d hydrology must be present,
	ucky Mineral (S1) <b>(LF</b>			(F17) <b>(MLRA 151</b>			disturbed or problematic.
-	leyed Matrix (S4)	(it 0, 0)		rtic (F18) <b>(MLRA</b>		unicss	distarbed or problematic.
	edox (S5)	•		oodplain Soils (F1		ιΔ)	
	Matrix (S6)			Bright Loamy Soils			30)
		T 11\	Anomalous i	Silgili Loamy Solls	(F20) (WLKA	1 149A, 155C, 15	(טפו
	face (S7) (LRR P, S,	1, 0)					
	ayer (if observed):						
Type:			=				
Depth (inc	:hes):		_			Hydric Soil Pre	esent? Yes No
Remarks:							

### WETLAND DETERMINATION DATA FORM – Atlantic and Gulf Coastal Plain Region

Project/Site:	City/Co	unty:		Sampling Date:
Applicant/Owner:			State:	Sampling Point:
Investigator(s):	Section	, Township, Range:		
Landform (hillslope, terrace, etc.):				
Subregion (LRR or MLRA):				
Soil Map Unit Name:				
Are climatic / hydrologic conditions on the sit				
Are Vegetation, Soil, or Hydr				
Are Vegetation, Soil, or Hydr	ology naturally problemati	ic? (If needed, o	explain any answers	s in Remarks.)
SUMMARY OF FINDINGS – Attac	h site map showing samp	oling point location	ons, transects,	important features, et
Hydrophytic Vegetation Present? Y	'es No			
	es No	Is the Sampled Area	V	M-
	'es No	within a Wetland?	Yes	No
Remarks:				
HYDROLOGY				
Wetland Hydrology Indicators:			Secondary Indicat	ors (minimum of two required)
Primary Indicators (minimum of one is requ	uired: check all that apply)		Surface Soil C	
Surface Water (A1)	Aquatic Fauna (B13)			etated Concave Surface (B8)
High Water Table (A2)	Marl Deposits (B15) (LRR	U)	Orainage Patt	
Saturation (A3)	Hydrogen Sulfide Odor (C		Moss Trim Lin	
Water Marks (B1)	Oxidized Rhizospheres ald			Vater Table (C2)
Sediment Deposits (B2)	Presence of Reduced Iron		Crayfish Burro	
Drift Deposits (B3)	Recent Iron Reduction in T	illed Soils (C6)	Saturation Vis	sible on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Thin Muck Surface (C7)		Geomorphic F	
Iron Deposits (B5)	Other (Explain in Remarks	)	Shallow Aquit	
Inundation Visible on Aerial Imagery (E	37)		FAC-Neutral	
Water-Stained Leaves (B9) Field Observations:			Spnagnum mo	oss (D8) <b>(LRR T, U)</b>
	No Depth (inches):			
	No Depth (inches):			
	No Depth (inches):		Hydrology Present	? Yes No
(includes capillary fringe)				100 110
Describe Recorded Data (stream gauge, m	onitoring well, aerial photos, previ	ious inspections), if ava	ailable:	
Remarks:				

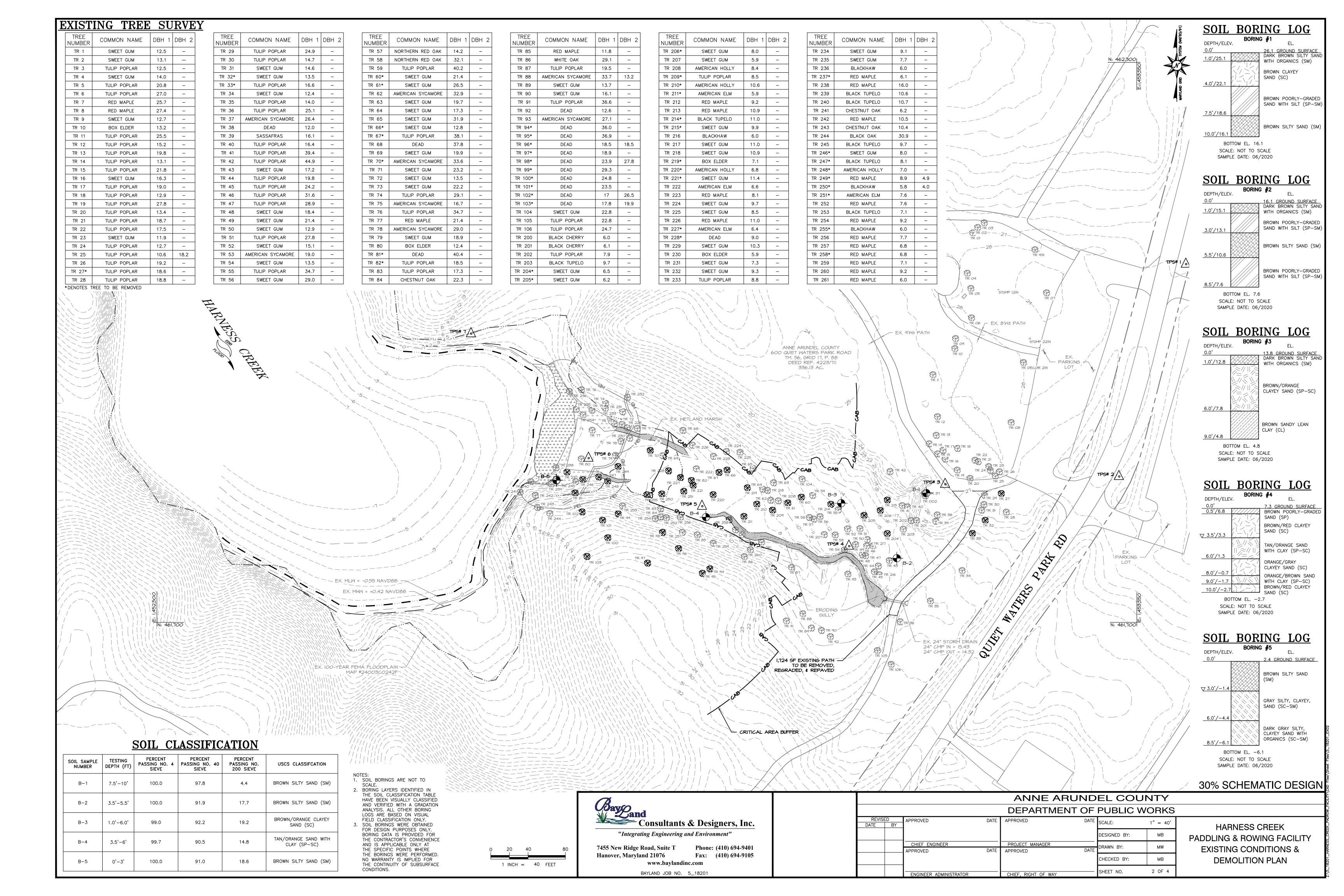
e Stratum (Plot size:)	Absolute % Cover	Dominant	Indicator	Dominance Test w	orksheet:		
	70 COVE		Status				
				Number of Dominal			(4)
				That Are OBL, FAC	, W, or FAC:	-	(A)
				Total Number of Do	minant		
				Species Across All	Strata:	-	(B)
				Percent of Dominar	nt Species		
				That Are OBL, FAC			(A/l
				Prevalence Index	workshooti		
						NA. déimhe he	
				Total % Cover			
		= Total Cov		OBL species			
50% of total cover:	20% of	total cover:		FACW species			
oling/Shrub Stratum (Plot size:)				FAC species	×	(3 =	
,				FACU species	×	(4 =	
				UPL species	x	< 5 =	
				Column Totals:	(/	A)	(E
				Prevalence In	dex = B/A =	·	
				Hydrophytic Vege	tation Indic	ators:	
				1 - Rapid Test	for Hydrophy	ytic Vegetatio	n
				2 - Dominance	Test is >50°	%	
				3 - Prevalence	Index is ≤3.0	0 <sup>1</sup>	
	:	= Total Cov	er	Problematic Hy	drophytic Ve	egetation¹ (Ex	(plain)
50% of total cover:	20% of	total cover:		<u> </u>	. ,	,	. ,
<u>b Stratum</u> (Plot size:)				<sup>1</sup> Indicators of hydric be present, unless			gy must
				Definitions of Fou	r Vegetation	n Strata:	
				Tuna Mandu plan	معالم بالمراجع	i	7.0)
				Tree – Woody plan more in diameter at			
				height.	. Drodot noigi	in (DDi i), 10g	ai aiooo
				Conline/Church \A	loody planta	. ovoludina vi	naa laa
				Sapling/Shrub – W than 3 in. DBH and			
					g. oato. t. a.	. 0.20 ()	
				Herb – All herbace			
				of size, and woody	plants less ti	nan 3.28 π tai	н.
				Woody vine – All v	voody vines	greater than	3.28 ft ir
				height.			
	:	= Total Cov	er				
50% of total cover:	20% of	total cover:					
ody Vine Stratum (Plot size:)							
				Hydrophytic			
	· · · · · · · · · · · · · · · · · · ·	= Total Cov		Vegetation Present?	Yes	No	
	20% of	total cover:					_

SOIL							Sampling Point:
Profile Desc	ription: (Describe	to the dep	th needed to docun	nent the indicator	or confirm	n the absence	of indicators.)
Depth	Matrix		Redox	k Features			
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u> Type <sup>1</sup>	<u>Loc<sup>2</sup></u>	Texture	Remarks

Depth	Matrix		Redo	x Features			
(inches)	Color (moist)	%	Color (moist)	%Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
							_
				- <del> </del>	<del>_</del>		
		<del></del>					
	ncentration, D=Deple				Grains.		=Pore Lining, M=Matrix.
Hydric Soil I	ndicators: (Applica	ble to all LR	Rs, unless othe	rwise noted.)		Indicators for	Problematic Hydric Soils <sup>3</sup> :
Histosol	(A1)	_	Polyvalue Be	elow Surface (S8)	(LRR S, T, U)	1 cm Mucl	k (A9) <b>(LRR O)</b>
	ipedon (A2)		-	urface (S9) (LRR \$			k (A10) <b>(LRR S)</b>
Black His				xy Mineral (F1) <b>(LF</b>			Vertic (F18) (outside MLRA 150A,B)
<del></del>	n Sulfide (A4)	•		ed Matrix (F2)	•		Floodplain Soils (F19) (LRR P, S, T)
	Layers (A5)	•	Depleted Ma				s Bright Loamy Soils (F20)
	Bodies (A6) (LRR P,	T, U)	Redox Dark			(MLRA	
	cky Mineral (A7) <b>(LRF</b>			rk Surface (F7)			nt Material (TF2)
	esence (A8) (LRR U)	, -, <b>-,</b>	Redox Depre				low Dark Surface (TF12)
<del></del>	ck (A9) (LRR P, T)	•	Nedox Bepit Marl (F10) <b>(I</b>				plain in Remarks)
<del></del>	Below Dark Surface	(A11)		hric (F11) (MLRA	151)	Other (EX	olain in remarks)
	rk Surface (A12)	(/ ( ) / )		nese Masses (F12)		7) <sup>3</sup> Indicato	rs of hydrophytic vegetation and
	airie Redox (A16) <b>(M</b> I	ΡΔ 150Δ)		ace (F13) <b>(LRR P</b> ,			d hydrology must be present,
	ucky Mineral (S1) <b>(LF</b>			(F17) <b>(MLRA 151</b>			disturbed or problematic.
-	leyed Matrix (S4)	(it 0, 0)		rtic (F18) <b>(MLRA</b>		unicss	distarbed or problematic.
	edox (S5)	•		oodplain Soils (F1		ιΔ)	
	Matrix (S6)			Bright Loamy Soils			(2D)
		T 11\	Anomalous i	Silgili Loamy Solls	(FZU) (IVILKA	1 149A, 155C, 15	(טפו
	face (S7) (LRR P, S,	1, 0)					
	ayer (if observed):						
Type:			=				
Depth (inc	:hes):		_			Hydric Soil Pre	esent? Yes No
Remarks:							

## **APPENDIX C**

Tree Survey Map and Inventory



TREE NUMBER	DBH, IN (SINGLE STEM)	COMMON NAME	CONDITION	Field Verified	REASON WHY NOT VERIFIED
TR 1	12.5	Sweet Gum	GOOD	YES	OUTSIDE OF WORK AREA
TR 2	13.1	Sweet Gum	FAIR	YES	OUTSIDE OF WORK AREA
TR 3	12.5	Tulip Poplar	GOOD	YES	OUTSIDE OF WORK AREA
TR 4	14.0	Sweet Gum	GOOD	YES	OUTSIDE OF WORK AREA
TR 5	20.8	Tulip Poplar	GOOD	YES	OUTSIDE OF WORK AREA
TR 6	27.0	Tulip Poplar	GOOD	YES	OUTSIDE OF WORK AREA
TR 7	25.7	Red Maple	GOOD	YES	OUTSIDE OF WORK AREA
TR 8	27.4	Red Maple	GOOD	YES	
TR 9	12.7	Sweet Gum	FAIR	YES	
TR 10	13.2	Box Elder	FAIR	YES	
TR 11	25.5	Tulip Poplar	GOOD	YES	
TR 12	15.2	Tulip Poplar	GOOD	YES	
TR 13	19.8	Tulip Poplar	GOOD	YES	
TR 14	13.1	Tulip Poplar	GOOD	YES	
TR 15	21.8	Tulip Poplar	GOOD	YES	
TR 16	16.3	Sweet Gum	FAIR	YES	
TR 17	19.0	Tulip Poplar	FAIR	YES	
TR 18	12.9	Tulip Poplar	GOOD	YES	
TR 19	27.8	Tulip Poplar	FAIR	YES	
TR 20	13.4	Tulip Poplar	FAIR	YES	
TR 21	18.7	Tulip Poplar	GOOD	YES	
TR 22	17.5	Tulip Poplar	GOOD	YES	
TR 23	11.9	Sweet Gum	FAIR	YES	
TR 24	12.7	Tulip Poplar	GOOD	YES	
TR 25	NA	Tulip Poplar	GOOD	YES	
TR 26	19.2	Tulip Poplar	GOOD	YES	
TR 27	18.6	Tulip Poplar	GOOD	YES	
TR 28	18.8	Tulip Poplar	FAIR	YES	
TR 29	24.9	Tulip Poplar	GOOD	YES	
TR 30	14.7	Tulip Poplar	FAIR	YES	
TR 31	14.6	Sweet Gum	FAIR	YES	
TR 32	13.5	Sweet Gum	FAIR	YES	
TR 33	16.6	Tulip Poplar	FAIR	YES	
TR 34	12.4	Sweet Gum	FAIR	YES	
TR 35	14.0	Tulip Poplar	GOOD	YES	
TR 36	25.1	Tulip Poplar	GOOD	YES	
TR 37	26.4	American Sycamore	GOOD	YES	

TR 38	12.0	DEAD	DEAD		
TR 39	16.1	Sassafras	FAIR	YES	
TR 40	16.4	Tulip Poplar	GOOD	YES	
TR 41	39.4	Tulip Poplar	FAIR	YES	
TR 42	44.9	Tulip Poplar	GOOD	YES	
TR 43	17.2	Sweet Gum	FAIR	YES	
TR 44	19.8	Tulip Poplar	POOR	YES	
TR 45	24.2	Tulip Poplar	FAIR	YES	
TR 46	31.6	Tulip Poplar	FAIR	YES	
TR 47	28.9	Tulip Poplar	FAIR	YES	
TR 48	18.4	Sweet Gum	GOOD	YES	
TR 49	21.4	Sweet Gum	GOOD	YES	
TR 50	12.9	Sweet Gum	GOOD	YES	
TR 51	27.8	Tulip Poplar	GOOD	YES	
TR 52	15.1	Sweet Gum	GOOD	YES	
TR 53	19.0	American Sycamore	POOR	YES	
TR 54	13.5	Sweet Gum	FAIR	YES	
TR 55	34.7	Tulip Poplar	GOOD	YES	
TR 56	29.0	Sweet Gum	FAIR	YES	
TR 57	14.2	Northern Red Oak	GOOD	YES	
TR 58	32.1	Northern Red Oak	POOR	YES	
TR 59	40.2	Tulip Poplar	FAIR	YES	
TR 60	21.4	Sweet Gum	GOOD	YES	
TR 61	26.5	Sweet Gum	GOOD	YES	
TR 62	32.9	American Sycamore	POOR	YES	
TR 63	19.7	Sweet Gum	GOOD	YES	
TR 64	17.3	Sweet Gum	GOOD	YES	
TR 65	31.9	Sweet Gum	GOOD	YES	
TR 66	12.8	Sweet Gum	GOOD	YES	
TR 67	38.1	Tulip Poplar	FAIR	YES	
TR 68	37.8	DEAD	DEAD		
TR 69	19.9	Sweet Gum	GOOD	YES	
TR 70	33.6	American Sycamore	POOR	YES	
TR 71	23.2	Sweet Gum	FAIR	YES	
TR 72	13.5	Sweet Gum	FAIR	YES	
TR 73	22.2	Sweet Gum	GOOD	YES	
TR 74	29.1	Tulip Poplar	FAIR	NO	OUTSIDE OF WORK AREA
TR 75	16.7	American Sycamore	POOR	NO	OUTSIDE OF WORK AREA
TR 76	34.7	Tulip Poplar	GOOD	NO	OUTSIDE OF WORK AREA
TR 77	21.4	Red Maple	GOOD	YES	
TR 78	29.0	American Sycamore	POOR	YES	

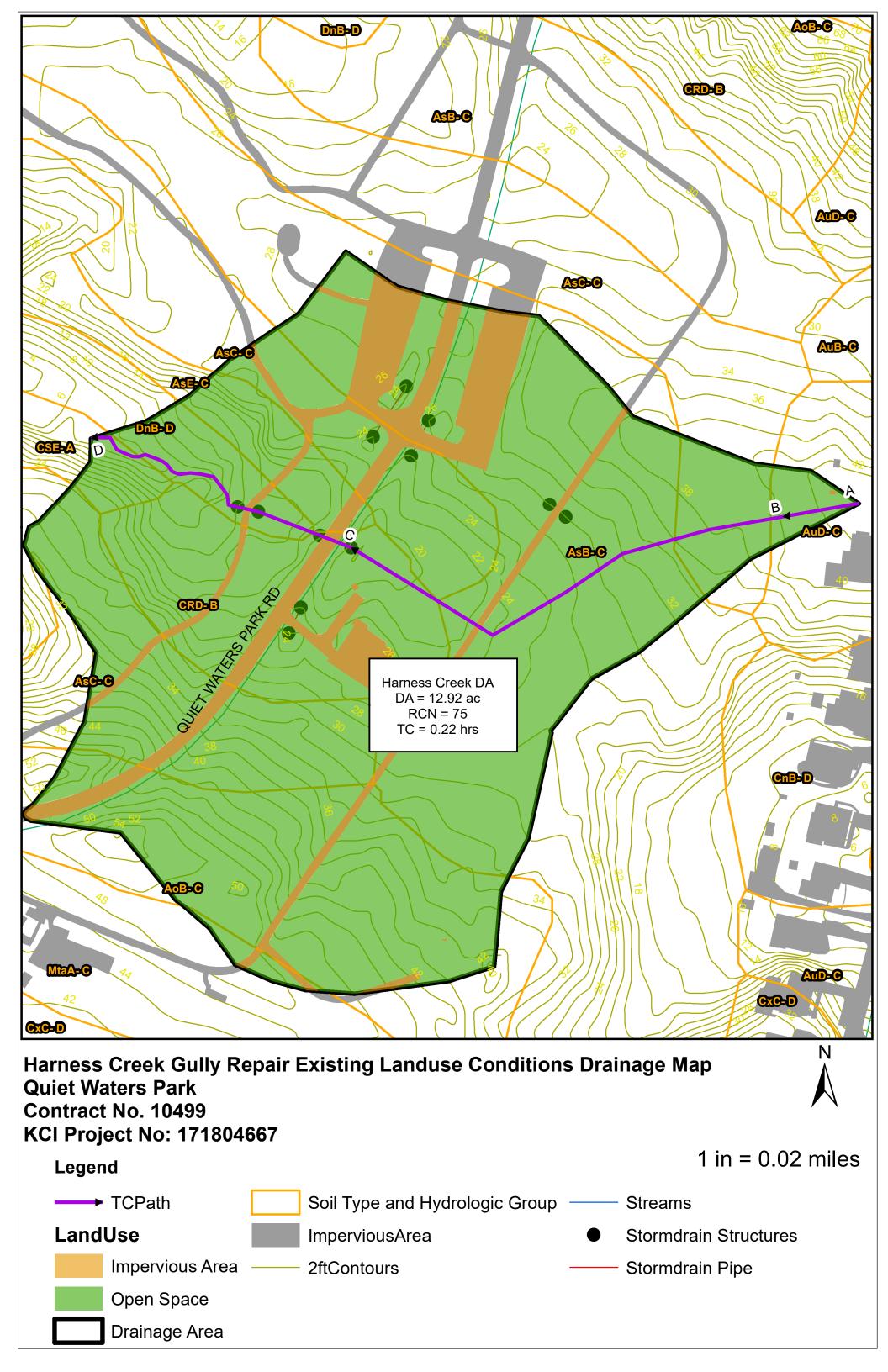
TR 79	18.9	Sweet Gum	GOOD	YES	
TR 80	12.4	Box Elder	FAIR	YES	
TR 81	40.4	DEAD	DEAD		
TR 82	18.5	Tulip Poplar	POOR	YES	
TR 83	17.3	Tulip Poplar	GOOD	YES	
TR 84	22.3	Chestnut Oak	FAIR	YES	
TR 85	11.8	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA
TR 86	29.1	White Oak	GOOD	NO	OUTSIDE OF WORK AREA
TR 87	19.5	Tulip Poplar	GOOD	NO	OUTSIDE OF WORK AREA
TR 88	NA	American Sycamore	POOR	NO	OUTSIDE OF WORK AREA
TR 89	13.7	Sweet Gum	GOOD	NO	OUTSIDE OF WORK AREA
TR 90	16.1	Sweet Gum	GOOD	NO	OUTSIDE OF WORK AREA
TR 91	36.6	Tulip Poplar	FAIR	NO	OUTSIDE OF WORK AREA
TR 92	12.6	DEAD	DEAD		
TR 93	27.1	American Sycamore	POOR	YES	
TR 94	36.0		DEAD		
TR 95	36.9		DEAD		
TR 96	NA		DEAD		
TR 97	18.9		DEAD		
TR 98	NA		DEAD		
TR 99	29.3		DEAD		
TR 100	24.8		DEAD		
TR 101	23.5		DEAD		
TR 102	NA		DEAD		
TR 103	NA		DEAD		
TR 104	22.8	Sweet Gum	GOOD	YES	
TR 105	22.8	Tulip Poplar	FAIR	NO	OUTSIDE OF WORK AREA
TR 106	24.7	Tulip Poplar	FAIR	NO	OUTSIDE OF WORK AREA
TR 107	55.0	Tulip Poplar	FAIR	ADDED	
TR 200	6.0	Black Cherry	FAIR	YES	
TR 201	6.1	Black Cherry	GOOD	YES	
TR 202	7.9	Tulip Poplar	GOOD	YES	
TR 203	9.7	Black Tupelo	GOOD	YES	
TR 204	6.5	Sweet Gum	GOOD	YES	
TR 205	6.2	Sweet Gum	GOOD	YES	
TR 206	8.0	Sweet Gum	GOOD	YES	
TR 207	5.9	Sweet Gum	GOOD	YES	
TR 208	8.4	American Holly	GOOD	YES	
TR 209	8.5	Tulip Poplar	GOOD	YES	
TR 210	10.6	American Holly	GOOD	YES	
TR 211	5.9	American Elm	GOOD	YES	

TR 212	9.2	Red Maple	GOOD	YES	
TR 213	10.9	Red Maple	GOOD	YES	
TR 214	11.0	Black Tupelo	FAIR	YES	
TR 215	9.9	Sweet Gum	GOOD	YES	
TR 216	6.0	Blackhaw	GOOD	YES	
TR 217	11.0	Sweet Gum	FAIR	YES	
TR 218	10.9	Sweet Gum	GOOD	YES	
TR 219	7.1	Box Elder	GOOD	YES	
TR 220	6.8	American Holly	GOOD	YES	
TR 221	11.4	Sweet Gum	GOOD	YES	
TR 222	6.6	American Elm	GOOD	YES	
TR 223	8.1	Red Maple	GOOD	YES	
TR 224	9.7	Sweet Gum	GOOD	YES	
TR 225	8.5	Sweet Gum	GOOD	YES	
TR 226	11.0	Red Maple	POOR	YES	
TR 227	6.4	American Elm	POOR	YES	
TR 228	9.0		DEAD		
TR 229	10.3	Sweet Gum	GOOD	YES	
TR 230	5.9	Box Elder	FAIR	YES	
TR 231	7.3	Sweet Gum	FAIR	NO	OUTSIDE OF WORK AREA
TR 232	9.3	Sweet Gum	GOOD	NO	OUTSIDE OF WORK AREA
TR 233	8.8	Tulip Poplar	GOOD	NO	OUTSIDE OF WORK AREA
TR 234	9.1	Sweet Gum	GOOD	NO	OUTSIDE OF WORK AREA
TR 235	7.7	Sweet Gum	GOOD	NO	OUTSIDE OF WORK AREA
TR 236	6.0	Blackhaw	FAIR	NO	OUTSIDE OF WORK AREA
TR 237	6.1	Red Maple	FAIR	YES	
TR 238	16.0	Red Maple	POOR	YES	
TR 239	10.6	Black Tupelo	GOOD	YES	
TR 240	10.7	Black Tupelo	GOOD	YES	
TR 241	6.2	Chestnut Oak	GOOD	YES	
TR 242	10.5	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA
TR 243	10.4	Chestnut Oak	GOOD	NO	OUTSIDE OF WORK AREA
TR 244	30.9	Black Oak	GOOD	NO	OUTSIDE OF WORK AREA
TR 245	9.7	Black Tupelo	GOOD	YES	
TR 246	8.0	Sweet Gum	GOOD	YES	
TR 247	8.1	Black Tupelo	GOOD	YES	
TR 248	7.0	American Holly	GOOD	YES	
TR 249	NA	Red Maple	GOOD	YES	
TR 250	NA	Blackhaw	GOOD	YES	
TR 251	7.6	American Elm	GOOD	YES	
TR 252	7.6	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA

TR 253	7.1	Black Tupelo	GOOD	NO	OUTSIDE OF WORK AREA
TR 254	9.2	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA
TR 255	6.0	Blackhaw	GOOD	YES	
TR 256	7.7	Red Maple	FAIR	YES	
TR 257	6.8	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA
TR 258	6.8	Red Maple	GOOD	YES	
TR 259	7.1	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA
TR 260	9.2	Red Maple	GOOD	NO	OUTSIDE OF WORK AREA
TR 261	6.0	Red Maple	GOOD	YES	
TR 262	8	Black Gum	GOOD	ADDED	
TR 263	6.0	American Holly	GOOD	ADDED	
TR 264	13.0	Sweet Gum	GOOD	ADDED	

# **Appendix C – Existing Hydrologic Analysis**

# C-1 Existing Conditions Drainage Area Map



# C-2 Existing Conditions TR-55 Analysis



# **TR-55 DESIGN COMPUTATIONS**

			011101111111111111111111111111111111111
Ву:	WBD	Project Name: Harness Creek	Project Number: 171804667.16
Date:	4/1/2022	County: Anne Arundel	<u></u>
Check:	YH	Drainage Area: 12.92 acres	Existing: X
Date:	4/1/2022	· · · · · · · · · · · · · · · · · · ·	Proposed:
Sheet	1 of 1	•	<del></del>

#### **WEIGHTED RUNOFF CURVE NUMBER**

Soil		Land Use or Zoning*	%		RCN		Area	RCN x Area
Group	No		Imperv.	Table 2-2	Figure 2-3	Figure 2-4	(Acre)	I KCIV X / II CU
Стоир	140.	Везсприон	Imperv.	Tubic 2 2	riguic 2 3	riguic 2 i	(ACIC)	
Α	3	Open Space (good) - grass >75%		39			0.18	6.93
В	3	Open Space (good) - grass >75%		61			1.61	98.20
В	4	Imperv paved parking lots,roofs,drives	100	98			0.29	28.39
С	3	Open Space (good) - grass >75%		74			9.27	686.20
С	4	Imperv paved parking lots,roofs,drives	100	98			1.15	112.56
D	3	Open Space (good) - grass >75%		80			0.40	32.28
D	4	Imperv paved parking lots,roofs,drives	100	98			0.01	1.39
			Total Caus	ro Miloci	0.02018	Total Acres	12.92	965.95
			Total Squa			Total Acres:	75	905.95
			Weighted	KCN=	74.78	, Use	/5	

\*Industrial land use category used for Institutional land use.

# TIME OF CONCENTRATION

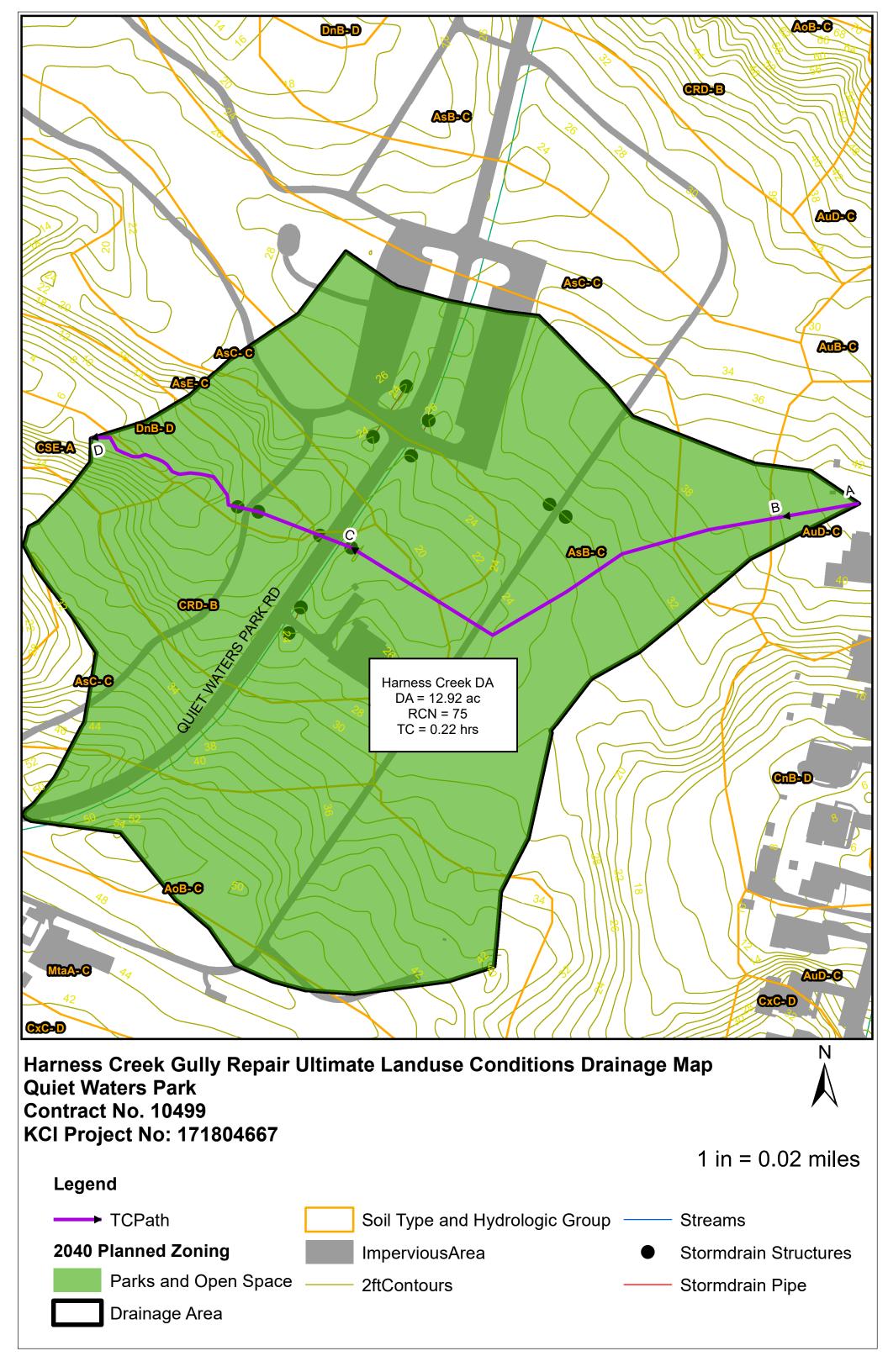
	<del>-                                    </del>		Type of Flow L(ft.) n A WP Slope Vel.									
ID		Туре	of Flow		L(ft.)	n	Α	WP	Slope	Vel.	Time	
									(Percent)	(fps)	(Hours)	
	She	et Flow										
A-B	5	Grass - short			100	0.150			3.2		0.137	
	Shal	llow Conc. Flow										
B-C		paved	Χ	unpaved	625				3.2	2.88	0.060	
		paved		unpaved								
		paved		unpaved								
		paved		unpaved								
		paved		unpaved								
	Cha	nnel or Storm I	Drain Flo	W								
C-D	1	Channel Flow,	d (ft) =	0.75	384	0.040	4.50	9.18	3.2	4.17	0.026	
										Total	0.22	

## **WATER QUALITY VOLUME**

P (in.)	Impervious Area to Treat** (ac.)	% Impervious	Rv	WQ <sub>v</sub> (acft.)	WQ <sub>v</sub> (cf.)
1.0	1.45	11.2%	0.151	0.163	7081

<sup>\*\*</sup> Impervious Area to Treat was estimated using the County's GIS Impervious layer.

# C-3 Ultimate Conditions Drainage Area Map



# C-4 Harness Creek Existing Conditions TR-20: SPSC Routing

# WinTR-20 Printed Page File Beginning of Input Data List M:\2018\171804667.16\Engr\Existing\HarnessCreek\_TR20.inp

Profile O	•	.20 e - TR20 T ing Condit		0	0	1.	0
SUB-AREA:	DAØ	0		0.020	75.	.22	
STREAM RE	ACH: 0	OUTLET	1.0		389.		
		001221			303.		
STORM ANA							
	1_yr_sm			2.66 3.22	TYPE NO_C TYPE NO_C		3.22
	2_yr_sm 10_yr_sm			5.01	TYPE NO_C		
	100_yr_sm	1		8.64	TYPE NO_C		
STREAM CR	OSS SECTIO	ıN:					
J	1.0	8.60					
		8.50	0.00	0.00	0.00	0.031	
		8.77 8.85	10.00	4.30	31.16	0.031	
		8.91	20.00 30.00	7.20 9.70	40.40 47.01	0.031 0.031	
		8.96	40.00	11.90	50.91	0.031	
		9.00	50.00	13.90	54.05	0.031	
		9.03	60.00	15.90	56.87	0.031	
		9.06 9.09	70.00 80.00	17.70 19.40	58.96 60.72	0.031 0.031	
				· • · •			

GLOBAL OUTPUT:

1. .25 YY N YY N

WinTR-20 Printed Page File End of Input Data List

Profile Output Table - TR20 Table Harness Creek Existing Conditions

# Name of printed page file: M:\2018\171804667.16\Engr\Existing\HarnessCreek\_TR20.out

# STORM 1\_yr\_sm

Reach	Area	ID or	Amount	Elevation (ft)	Time	Rate	Rate
DA0	0.020		0.420		12.20	9.3	462.70
Line Start Time		Flow	Values @ ti	ime increment	t of 0.	250 hr	
(hr)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
11.750 13.500		2.8		3.8	2.2	1.7	1.3
				Elevation (ft)			
0	0.020	Upstream	0.420	8.75	12.20	9.3	462.70
			•	ime increment (cfs)			
11.750 13.500		2.8	8.4	3.8	2.2	1.7	1.3
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
Reach	Area	ID or	Amount	Elevation (ft)	Time	Rate	Rate
0	0.020	Downstream	0.412	8.75	12.23	9.2	461.79

			Values @ tin				
(nr)	(CTS)	(CTS)	(cfs)	(CTS)	(CTS)	(CTS)	(CTS)
11.750 13.500		2.2	9.1	4.1	2.4	1.8	1.4
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
			Amount				
			(in)				
	· · · /		` ,	` ,	` ,	` ,	` ,
OUTLET	0.020		0.412		12.23	9.2	461.79
WinTR-20 V ↑	ersion 3.20	Profile	Page Output Tabl	le - TR20 Ta	ble	04/01/202	22 15:04
		Harness	Creek Exist	ting Conditi	ons		
Line							
Start Time			Values @ tin				
Start Time			Values @ tin (cfs)				
Start Time (hr)	(cfs) 0.0	(cfs)		(cfs)	(cfs)	(cfs)	(cfs)
Start Time (hr) 11.750	(cfs) 0.0	(cfs) 2.2	(cfs)	(cfs) 4.1	(cfs) 2.4	(cfs)	(cfs)
Start Time (hr) 11.750 13.500	(cfs) 0.0 1.1	(cfs) 2.2 0.0	(cfs) 9.1	(cfs) 4.1 STORM 2_yr_	(cfs) 2.4 sm	(cfs) 1.8	(cfs) 1.4
Start Time (hr) 11.750 13.500  Area or	(cfs) 0.0 1.1 Drainage	(cfs) 2.2 0.0  Rain Gage	(cfs) 9.1 Runoff	(cfs) 4.1 STORM 2_yr_	(cfs) 2.4 sm Peak	(cfs) 1.8 Flow	(cfs) 1.4
Start Time (hr) 11.750 13.500 Area or Reach	(cfs) 0.0 1.1 Drainage Area	(cfs) 2.2 0.0  Rain Gage ID or	(cfs) 9.1 Runoff Amount	(cfs) 4.1  STORM 2_yr_ Elevation	(cfs) 2.4 sm Peak Time	(cfs)  1.8  Flow Rate	(cfs) 1.4 Rate
Start Time (hr) 11.750 13.500 Area or Reach	(cfs) 0.0 1.1 Drainage	(cfs) 2.2 0.0  Rain Gage ID or	(cfs) 9.1 Runoff	(cfs) 4.1  STORM 2_yr_ Elevation	(cfs) 2.4 sm Peak Time	(cfs)  1.8  Flow Rate	(cfs) 1.4
Start Time (hr) 11.750 13.500 Area or Reach	(cfs) 0.0 1.1 Drainage Area	(cfs) 2.2 0.0  Rain Gage ID or	(cfs) 9.1 Runoff Amount	(cfs) 4.1  STORM 2_yr_ Elevation	(cfs) 2.4 sm Peak Time	(cfs)  1.8  Flow Rate (cfs)	(cfs) 1.4 Rate (csm)
Start Time (hr)  11.750 13.500  Area or Reach Identifier	(cfs) 0.0 1.1 Drainage Area (sq mi)	(cfs) 2.2 0.0  Rain Gage ID or	(cfs) 9.1 Runoff Amount (in)	(cfs) 4.1  STORM 2_yr_ Elevation	(cfs) 2.4 sm Peak Time (hr)	(cfs)  1.8  Flow Rate (cfs)	(cfs) 1.4Rate (csm)
Start Time (hr)  11.750 13.500  Area or Reach Identifier DA0	(cfs) 0.0 1.1 Drainage Area (sq mi) 0.020	(cfs) 2.2 0.0  Rain Gage ID or Location	(cfs) 9.1 Runoff Amount (in)	(cfs) 4.1  STORM 2_yr_ Elevation (ft)	(cfs) 2.4 sm Peak Time (hr) 12.18	(cfs)  1.8  Flow Rate (cfs)  14.3	(cfs) 1.4 Rate (csm) 714.86
Start Time (hr)  11.750 13.500  Area or Reach Identifier  DA0  Line	(cfs)  0.0  1.1  Drainage Area (sq mi)  0.020	(cfs) 2.2 0.0  Rain Gage ID or Location	(cfs) 9.1  Runoff Amount (in) 0.732	(cfs) 4.1  STORM 2_yr_ Elevation (ft)	(cfs) 2.4 sm Peak Time (hr) 12.18 of 0.2	(cfs) 1.8  Flow Rate (cfs) 14.3	(cfs) 1.4 Rate (csm) 714.86
Start Time (hr)  11.750 13.500  Area or Reach Identifier  DA0  Line Start Time (hr)	(cfs)  0.0  1.1  Drainage Area (sq mi)  0.020  (cfs)	(cfs)  2.2 0.0  Rain Gage ID or Location  Flow (cfs)	(cfs) 9.1  Runoff Amount (in) 0.732  Values @ tin (cfs)	(cfs) 4.1  STORM 2_yr_ Elevation (ft)  me increment (cfs)	(cfs) 2.4  sm Peak Time (hr) 12.18  of 0.2 (cfs)	(cfs)  1.8  Flow Rate (cfs)  14.3  250 hr (cfs)	(cfs) 1.4 Rate (csm) 714.86 (cfs)
Start Time (hr)  11.750 13.500  Area or Reach Identifier  DA0  Line Start Time	(cfs)  0.0 1.1  Drainage Area (sq mi)  0.020  (cfs)  0.0	(cfs)  2.2 0.0  Rain Gage ID or Location  Flow (cfs) 1.5	(cfs) 9.1  Runoff Amount (in) 0.732  Values @ tim	(cfs) 4.1  STORM 2_yr_ Elevation (ft)	(cfs) 2.4  sm Peak Time (hr) 12.18  of 0.2 (cfs) 5.5	(cfs)  1.8  Flow Rate (cfs)  14.3  250 hr (cfs)  3.2	(cfs) 1.4 Rate (csm) 714.86
Start Time (hr)  11.750 13.500  Area or Reach Identifier  DA0  Line Start Time (hr)  11.500 13.250	(cfs)  0.0 1.1  Drainage Area (sq mi)  0.020  (cfs)  0.0 1.9	(cfs)  2.2 0.0  Rain Gage ID or Location  Flow (cfs)  1.5 1.5	(cfs) 9.1  Runoff Amount (in) 0.732  Values @ tin (cfs) 4.9 1.3	(cfs) 4.1  STORM 2_yr_ Elevation (ft)  me increment (cfs) 12.7 1.2	(cfs) 2.4  sm Peak Time (hr) 12.18  of 0.2 (cfs) 5.5 1.1	(cfs)  1.8  Flow Rate (cfs)  14.3  250 hr (cfs)  3.2 0.0	(cfs) 1.4 Rate (csm) 714.86 (cfs) 2.4
Start Time (hr)  11.750 13.500  Area or Reach Identifier  DA0  Line Start Time (hr)  11.500	(cfs)  0.0 1.1  Drainage Area (sq mi)  0.020  (cfs)  0.0 1.9	(cfs)  2.2 0.0  Rain Gage ID or Location  Flow (cfs) 1.5	(cfs) 9.1  Runoff Amount (in) 0.732  Values @ tim (cfs) 4.9	(cfs) 4.1  STORM 2_yr_ Elevation (ft)  me increment (cfs) 12.7 1.2	(cfs) 2.4  sm Peak Time (hr) 12.18  of 0.2 (cfs) 5.5 1.1 Peak	(cfs)  1.8  Flow Rate (cfs)  14.3  250 hr (cfs)  3.2	(cfs) 1.4 Rate (csm) 714.86 (cfs) 2.4

(in)

Location

(ft)

(hr)

(cfs)

(csm)

Identifier (sq mi)

0	0.020	Upstream	0.732	8.80	12.18	14.3	714.86
Line Stant Time		Elow	Values @ ti	ma increment	- of 0.3	050 hn	
			(cfs)				
			4.9 1.3				
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
Reach	Area	ID or	Amount	Elevation	Time	Rate	Rate
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
0	0.020	Downstream	0.724	8.80	12.23	14.3	714.36
Line							
			Values @ ti				
(nr)	(CTS)	(CTS)	(cfs)	(CTS)	(CTS)	(CTS)	(CTS)
11.750	0.4	4.0	13.9	5.9	3.4	2.5	1.9
13.500	1.6	1.3	1.2	1.1	0.0		
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
Reach	Area	ID or	Amount	Elevation	Time	Rate	Rate
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
OUTLET	0.020		0.724		12.23	14.3	714.36
WinTR-20 Ve	ersion 3.2	0	Page	2		04/01/202	22 15:04
<i>T</i>			e Output Tab s Creek Exis				
				8			
Line Stant Time		Elow	Values @ ti	mo increment	- of 0 ^	DEQ hn	
			(cfs)				
11.750 13.500			13.9 1.2		3.4 0.0		1.9
13.300	1.0	1.5	1.2	1.1	0.0		
				STORM 10_yr	_sm		
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
Reach	Area	ID or	Amount	Elevation	Time	Rate	Rate
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
DA0	0.020		2.026		12.18	32.7	1634.51

			Values @ time				
(111 )	(013)	(013)	(613)	(013)	(013)	(013)	(013)
10.750	0.0	1.1	1.6	2.5	4.9	13.2	28.3
12.500	11.5	6.5	4.9	3.8		2.5	2.3
14.250	2.1		1.7	1.6			1.3
16.000	1.3	1.2	1.2	1.1	1.1	1.0	0.0
Area or	Drainage	Rain Gage	Runoff		Peak F	:1ow	
			Amount				
			(in)				
0			2.026				1634.51
Line Stant Time		Elow	Values @ time	increment	of 0.25	60 hn	
			(cfs)				
(111 )	(013)	(013)	(613)	(013)	(013)	(013)	(013)
10.750	0.0	1.1	1.6	2.5	4.9	13.2	28.3
12.500	11.5	6.5	4.9	3.8	3.0	2.5	2.3
	2.1		1.7				
	1.3		1.2			1.0	
	_					_	
Area or							
Reach	Area	ID or		Elevation			
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
0	0.020	Downstream	2.017	8.92	12.21	32.7	1634.51
Line							
Start Time		Flow	Values @ time	increment	of 0.25	60 hr	
(hr)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
10 750	0.0	1.0	1.6	2.4	4.6	11 4	20.0
			1.6				
12.500				3.8	3.1	2.5	2.3
14.250 16.000				1.6 1.1	1.4 1.1	1.4 1.0	
16.000	1.5	1.2	1.2	1.1	1.1	1.0	0.0
WinTR-20 Vo	ansion 3 2	a	Page 3			04/01/202	)2 15·0/
MIIIIN-20 V	. 3±011 J.Z	•	i age 3	,		O-7/ O1/ 202	-2 13.04
			e Output Table s Creek Existi				
Area or	Dnainago	Rain Gage	Runoff		Dook 5	:1ow -	
Reach	Area	ID or		Elevation		Rate	
Identifier				(ft)	(hr)		
TOGILCTITEL	(34 1111)	LUCACIUII	(111)	(10)	(111)	(013)	(CSIII)

OUTLET	0.020		2.017		12.21	32.7	1634.51
Line Start Time		Flow	Values @ time	increment	of 0.2	250 hr	
			(cfs)				
			1.6				
			5.0				
14.250	2.1	1.9		1.6		1.4	
16.000	1.3	1.2	1.2	1.1	1.1	1.0	0.0
			S	TORM 100_y	r_sm		
			Runoff				
Reach	Area	ID or	Amount	Elevation	Time	Rate	Rate
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
DA0			5.516			74.1	
Line							
		Flow	Values @ time	increment	of 0.2	250 hr	
			(cfs)				
9.250			1.4				
			7.5				
			7.7				
14.500		3.5					
16.250							
18.000			1.6				
19.750				1.4	1.4	1.3	
21.500					1.2	1.2	1.2
23.250	1.1	1.1	1.1	1.1	0.0		
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
Reach		ID or	Amount	Elevation	Time	Rate	Rate
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
0	0.020	Upstream	5.516	9.07	12.18	74.1	3706.13
Line							
Start Time		Flow	Values @ time	increment	of 0.2	250 hr	
(hr)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
9.250	0.0			1.7	2.0	2.3	2.9
11.000	3.9			13.6	32.9	62.8	24.4
12.750	13.4		7.7	6.2	5.0	4.6	4.2
14.500	3.8			2.8	2.7	2.6	2.5
16.250	2.4			2.1	2.0	1.9	1.8
18.000	1.7	1.6	1.6	1.6	1.5	1.5	1.5

19.750 21.500			1.4 1.3				1.3 1.2
WinTR-20 Ve	ersion 3.20	9	Page	4		04/01/20	22 15:04
			e Output Tal s Creek Exi				
Line Start Time		Flow	Values @ t:	ime increme	ent of a	250 hr	
			(cfs)				
23.250	1.1	1.1	1.1	1.1	0.0		
Area or	Drainage	Rain Gage					
Reach	Area	ID or	Amount	Elevatio	on Time	Rate	Rate
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
0	0.020	Downstream	5.507	9.07	12.21	73.9	3696.16
Line							
Start Time			Values @ t:				
(hr)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
9.500	0.5						
11.250							
13.000	10.2		6.3				
14.750	3.5		2.8			2.5	
16.500	2.3						
18.250	1.6				1.5		
20.000	1.5				1.4		
21.750	1.3				1.2	1.2	1.1
23.500	1.1	1.1	1.1	0.0			
Area or	Drainage	Rain Gage	Runoff		Peak	Flow	
			Amount				
Identifier	(sq mi)	Location	(in)	(ft)	(hr)	(cfs)	(csm)
OUTLET	0.020		5.507		12.21	73.9	3696.16
Line							
Start Time			•				
(hr)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
9.500	0.5						3.8
11.250	5.3						
13.000	10.2				4.6		3.9
14.750	3.5		2.8	2.7	2.6		2.4
16.500	2.3						
18.250	1.6	1.6	1.6	1.5	1.5	1.5	1.5

20.000	1.5	1.4	1.4	1.4	1.4	1.3	1.3
21.750	1.3	1.3	1.2	1.2	1.2	1.2	1.1
23.500	1.1	1.1	1.1	0.0			

WinTR-20 Version 3.20

Page 5

04/01/2022 15:04

Profile Output Table - TR20 Table Harness Creek Existing Conditions

Area or	Drainage		Peak	Flow by St	orm	
Reach	Area	1_yr_sm	2_yr_sm	10_yr_sm	100_yr_sm	
Identifier	(sq mi)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)
DA0	0.020	9.3	14.3	32.7	74.1	
0	0.020	9.3	14.3	32.7	74.1	
DOWNSTREAM		9.2	14.3	32.7	73.9	
OUTLET	0.020	9.2	14.3	32.7	73.9	

# **Appendix D – Design Computations**



# KCI Technologies, Inc.

Project Name: Harness Creek Originator: WBD

County: Anne Arundel Date: 4/5/2022

Project Number: 171804667.16 Reviewed By: BE

Date: 4/6/2022

SPSC Riffle Sizing Spreadsheet (Based on Anne Arundel County SPSC Guidelines, 2021)

Designer must select/input
Calculated value/Designer shall not change
Default values provided. Advanced designer may change to customize to site specific design

Riffle Grade Control Sizing					
	Q <sub>100</sub>	Q <sub>10</sub>	$Q_2$		
Design Flow (cfs)	74.1	32.7	14.3		
Width (ft)	16.0	16.0	16.0		
L, Length (ft)	8.0	8.0	8.0		
H, Height (ft)	1.0	1.0	1.0		
Design Depth of flow (ft)	0.92	0.9	0.9		
D50 (in)	9	9	9		
P <sub>D</sub> , Parabolic Depth (ft)	0.92	0.92	0.92		
Degree of incision (W/P <sub>D</sub> )	17.4	17.4	17.4		
Manning's n Value	0.050	0.1	0.1		
Slope (ft/ft)	0.1	0.1	0.1		
Rock Unit Weight (lbs/cf)	165.0	165.0	165.0		
Top Width at Depth	16.0	16.0	16.0		
Flow area (sf)	9.8	9.8	9.8		
Hydraulic Radius	0.61	0.61	0.61		
Froude	1.4	1.1	1.1		
Isbash Maximum Velocity (ft/s)	7.7	7.7	7.7		
Depth ("A") at TW/4 offset from centerline	0.7	0.7	0.7		
Calculated Flow at Design Depth (cfs)	74.2	59.9	59.9		
Calculated Velocity (ft/s)	7.6	6.1	6.1		
Does the proposed section provide adequate conveyance?	YES	YES	YES		
Is the proposed velocity less than the maximum allowable velocity?	YES	YES	YES		

Maximum allowable riffle stone size for a given Q100			
Q100, cfs ≤	Max D50, inches		
15	6		
125	9		
500	12		
1500	18		
2000	24		



# KCI Technologies, Inc.

Project Name: Harness Creek
County: Anne Arundel

171804667.16 Reviewed By: Date:

Originator:

Date:

WBD 4/8/2022 BE

4/8/2022

SPSC Cascade Sizing Spreadsheet (Based on Anne Arundel County SPSC Guidelines, 2021)

Designer must select/input

Calculated value/Designer shall not change

Default values provided. Advanced designer may change to customize to site specific design

Project Number:

Case	cade Sizing		
	Q <sub>100</sub>	Q <sub>10</sub>	$Q_2$
Design Flow (cfs)	74.1	32.7	14.3
Width (ft)	16.0	16.0	16.0
L, Length (ft)	8.0	8.0	8.0
H, Height (ft)	2.0	2.0	2.0
Design Depth of flow (ft)	0.92	0.9	0.9
D50 (in)	30	30	30
P <sub>D</sub> , Parabolic Depth (ft)	0.92	0.92	0.92
Degree of incision (W/P <sub>D</sub> )	17.4	17.4	17.4
Manning's n Value	0.050	0.050	0.050
Slope (ft/ft)	0.3	0.3	0.3
Rock Unit Weight (lbs/cf)	165.0	165.0	165.0
Top Width at Depth	16.0	16.0	16.0
Flow area (sf)	9.8	9.8	9.8
Hydraulic Radius	0.61	0.61	0.61
Froude	2.0	2.0	2.0
Isbash Maximum Velocity (ft/s)	14.0	14.0	14.0
Depth ("A") at TW/4 offset from centerline	0.7	0.7	0.7
Calculated Flow at Design Depth (cfs)	104.9	104.9	104.9
Calculated Violocity (ft/s)	104.5	104.5	104.5
Does the proposed section provide adequate conveyance?	YES	YES	YES
Is the proposed velocity less than the maximum allowable velocity?	YES	YES	YES
Does the proposed cascade have a slope of <= 0.5 ft/ft?	YES		

Scour Depth - pools downstream of cascades				
Q <sub>100</sub> , cfs	74.1			
H, Height of upstream grade control structure, ft	2.0			
TW, Top width of the upstream grade control				
structure, ft	16.0			
y, depth of Q <sub>100</sub> in downstream/receiving structure	0.92			
K, coefficient	1.32			
p <sub>d</sub> , Calculated scour depth, ft	2.6			
Minimum footer boulder depth below pool				
bottom, ft	2.0			

 Project #:
 71804667.16
 BY:
 WBD
 4/18/2022

 Project Name: Harness Creek Gully Repair
 CHECK:
 BLE
 4/18/2022

#### **Proposed Pool Storage for Runoff Volume Reduction**

#### Volume Stored in Pools

	Pool Bottom Elevation	U/S Pool Bottom Area	U/S Pool Top Area	Volume
Structure	(ft)	(ft <sup>2</sup> )	(ft <sup>2</sup> )	(ft <sup>3</sup> )
RW1	-1	168.9	561.4	730
RW2	0	141.9	510.2	652
RW3	1	205.5	623.9	829
RW4	2	168.5	559.6	728
RW5	3	114.2	469.9	584
RW6	4	248.5	697.2	946
RW7	5	290.0	774.6	1065
RW8	6	47.0	333.1	380
RW9	7	46.0	325.6	372
RW10	7	21.3	379.8	401
C1	10	119.8	470.6	590
RW11	11	0.4	192.5	193
RW12	12	61.2	225.8	287

Total Volume Stored in Pools =

7,758 ft<sup>3</sup>

**Project:** 

### **Harness Creek Gully Repair**

BY: WBD CHECKED: BLE 4/19/2022 4/19/2022

# **Upland Structural BMP Impervious Acre Credits & Pollutant Load Reductions**

Reference: Accounting for Stormwater Wasteload Allocations and Impervious Acres Treated: Guidance for National Pollutant Discharge Elimination System Stormwater Permits. June, 2020. Maryland Department of the Environment.

### **Impervious Credit Acres:**

Total Drainage Area to BMP = 12.92 ac
Total Untreated Impervious Area to BMP = 1.45 ac

Pervious Area to BMP = 11.47 ac

WQv Target (1 in. Rainfall Depth Treated) = 7,081 cf 0.16 ac-ft WQv Provided = 7,758 cf 0.18 ac-ft

% of Target = 109.56 %

Max. WQv Provided = 7,758 cf

Rainfall Depth Treated ( $P_E$ ) (Max. 3 in.) = 1.10 in.

 $WQ_T$  Credit = 1.02 in.

Impervious Area Treated = 1.48 ac

## Annual Nutrient Load Reduction (lbs/yr):

Load Reduction (lbs/yr) = [Urban Unit Load (lbs/acre/yr)]  $\times$  [Impervious Surface in BMP Drainage Area (acres)]  $\times$  [BMP Efficiency/100]  $\times$  [Phase 6 Modeling Segment Delivery Factor]

#### Urban Unit Load (lbs/ac/vr):

t 20dd (100) doj y 1 j .				
	Acres in BMP Drainage	Statewide EOS Urban Unit Load		
Load Source	Area	TN	TP	TSS
Aggregate Impervious		20.09	2.55	8,474
Impervious Road	1.45	35.79	6.95	17,328
Mixed Open	3.81	8.15	1.59	1,414
Septic		16.66	0.00	0
Tree Canopy over Impervious		32.75	6.19	16,115
Turf		13.35	2.12	1,414
Tree Canopy over Turf		10.18	1.62	1,332
True Forest	7.66	2.28	0.32	719
Total Urban		12.89	1.46	3,306
Total:	12.92	7.77	1.44	2,788

	TN	TP	TSS	
BMP Efficiency =	61.0	71.4	76.5	](
Urban Unit Load (lbs/ac/yr) =	7.77	1.44	2,788	](
Edge of Tide Loading Factor =	1	1	1	(
Load (lb/yr) =	11.27	2.09	4,043	]
Load Reduction (lb/yr) =	6.88	1.49	3,094	l
Load Post-Retrofit (lb/yr) =	4.39	0.60	949	]

(Table 3) BMP Type = (Table 4)

(MDE EOT Factor Map)

Table 2. Stormwater BMPs for Upland Applications

Runo	ff Reduction (RR) Practices	Stor	mwater Treatment (ST) Practices
Manual Reference	Practice	Manual Reference	Practice
÷	Infiltration		Ponds
M-3	Landscape Infiltration	P-1	Micro-Pool Extended Detention (ED)
M-4	Infiltration Berm	P-2	Wet Pond
M-5	Dry Well	P-3	Wet ED Pond
55	Filtering Systems	P-4	Multiple Pond
F-6	Bioretention <sup>1</sup>	P-5	Pocket Pond
M-2	Submerged Gravel Wetland		Wetlands <sup>2</sup>
M-6	Micro-Bioretention <sup>1</sup>	W-1	Shallow Wetland
M-7	Rain Garden	W-2	ED Shallow Wetland
M-9	Enhanced Filter	W-3	Pond/Wetland System
72	Open Channel Systems	W-4	Pocket Wetland
O-1	Dry Swale		Infiltration <sup>2</sup>
M-8	Grass Swale	I-1	Infiltration Trench
M-8	Bio-Swale	I-2	Infiltration Basin
M-8	Wet Swale Filtering Systems		
	Alternative Surfaces	F-1	Surface Sand Filter
A-1	Green Roof	F-2	Underground Filter
A-2	Permeable Pavement	F-3	Perimeter Filter

Table 3. TN, TP, and TSS Removal Efficiencies for Upland BMPs

Rainfall Depth Treated	TN Removal TSS Removal Efficiency (%)							emoval ncy (%)
(inches)	RR	ST	RR	ST	RR	ST		
0.00	0.00	0.00	0.00	0.00	0.00	0.00		
0.20	23.3	13.6	29.1	27.2	27.2	21.4		
0.40	39.2	22.8	48.9	45.7	45.7	35.9		
0.60	49.3	28.8	61.7	57.5	57.5	45.2		
0.80	55.7	32.5	69.7	65.1	65.1	51.1		
1.00	59.7	35.0	74.9	69.9	69.9	54.9		
1.20	62.5	36.5	78.3	73.0	73.0	57.4		
1.40	64.4	37.6	80.7	75.2	75.2	59.1		
1.60	65.6	38.4	82.3	76.7	76.7	60.3		
1.80	66.4	38.8	83.3	77.6	77.6	61.0		
2.00	66.8	39.1	83.9	78.2	78.2	61.4		
2.20	67.1	39.2	84.2	78.4	78.4	61.7		
2.40	67.5	39.3	84.6	78.6	78.6	61.9		
$2.60^{1}$	67.9	39.4	85.0	78.8	78.8	62.1		
$2.80^{1}$	68.3	39.5	85.4	79.0	79.0	62.3		
$3.00^{1}$	68.6	39.6	85.8	79.2	79.2	62.5		

Note:

<sup>1</sup> Values exceed the adjustor curves and are extrapolated from the CBP formulas.

Table 4. Statewide Edge-of-Stream Urban Unit Load Summary

Statewide EOS Urban Unit Load (lbs/acre/yr			
TN	TP	TSS	
20.09	2.55	8,474	
35.79	6.95	17,328	
8.15	1.59	1,414	
16.66	0.00	0.00	
32.75	6.19	16,115	
13.35	2.12	1,414	
10.18	1.62	1,332	
2.28	0.32	719	
12.89	1.46	3,306	
	TN 20.09 35.79 8.15 16.66 32.75 13.35 10.18 2.28	TN TP  20.09 2.55  35.79 6.95  8.15 1.59  16.66 0.00  32.75 6.19  13.35 2.12  10.18 1.62  2.28 0.32	

Note

<sup>&</sup>lt;sup>1</sup> For more information on Load Sources in the Phase 6 Model, see Appendix B.

### **Protocol 5 Credit Computations**

**Project Name: Harness Creek** By: BLE

Project Number: 171804667.16 Check:

#### **Base Level Controls**

Upstream Control Point = Outfall

Upstream Control Point Elevation = 14.41 ft

> If upstream limits of erosion if outfall is not present, use L<sub>max</sub>.  $L_{max} = 153 A_d^{0.6}$

710

Downstream Control Point = Confluence with Harness Creek

Downstream Control Point Elevation = 0 ft

Total Length = 457 ft

Existing Channel Slope = 0.0315 ft/ft

Note: If existing slope is within 5% of the equilibrium slope calculated for existing conditions, this portion of the channel is considered stable base level control.

> XS 1 XS 2 XS3 Average 4.2 Bottom Width = 6.8 5.7 ft 6.0

# **Equilibrium Bed Slope**

#### **Cohesive Beds:**

Simon and Thomas: where

> S = Equilibrium Slope (ft/ft); $S = 0.0028A^{-0.33}$

A = Drainage Area (km<sup>2</sup>)

Drainage Area (A) = 12.92 ac =  $0.052 \text{ km}^2$ 

S = 0.0074 ft/ft

### **Beds Coarser than Sand:**

Pebble Count:

	(mm)	(ft)
D16		0.000
D35		0.000
D50	1	0.003
D84		0.000
D90		0.000
D95		0.000

Mean Grain Size  $(D_m) =$ mm

> 0.045 (Estimated from field) n =

10.5 cfs (Usually Bankfull Q or Q<sub>1.5</sub>) Channel Forming Discharge =

Average Channel Width = 5.7

Channel Forming Discharge per Unit Width (q) = ft<sup>2</sup>/s 1.85

### Beds of Sand and Fine Gravel (0.1 - 5 mm) (No Bed-Material Sediment Supplied from Upstream):

Pemberton and Lara:

where

$$S_{eq} = \left(\frac{\tau_c}{\gamma_w y}\right)$$

 $S_{eq} = Equilibrium Slope (ft/ft);$   $\tau_c = Critical Shear Stress (lb/ft^2);$  $\gamma_w = Specific Weight of Water (lb/ft^3);$ 

y = Mean Flow Depth (ft)

Critical Shear Stress =

0.062

lb/ft<sup>2</sup> (From Figure TS14B-9)

Specific Weight of Water =

62.4 lb/ft<sup>3</sup>

		Flow Depth (ft) <sup>2</sup>				
Storm Event	Q (cfs) <sup>1</sup>	XS 1	XS 2	XS 3	Average	S <sub>eq</sub> (ft/ft)
Bankfull	-	0.59	0.52	0.63	0.58	0.0017
1.25-Year	10.5	0.59	0.52	0.63	0.58	0.0017
2-Year	14.3	0.72	0.62	0.75	0.70	0.0014
10-Year	32.7	1.18	1.01	1.2	1.13	0.0008
100-Year	74.1	1.9	1.59	1.87	1.79	0.0005

<sup>&</sup>lt;sup>1</sup>Q determined from TR-20 or StreamStats.

Selected Equilibrium Slope: S<sub>eq</sub> = 0.0017 ft/ft

### **Equilibrium Bank Slope**

- No Seepage Condition: Equilibrium bank slopes are in the range of 1.4:1 to 2.1:1 for banks comprised of sand and 1.9:1 for silt.
- Seepage Flowing Generally Parallel to Slope Condition: Stable bank slopes are in the range of 2.6:1 to 4.1:1 for banks comprised of sand and 3.9:1 for silt.
- Seepage Generally Flowing along Horizontal Flow Paths Condition: Stable bank slopes are in the range of 2.9:1 to 4.4:1 for banks comprised of sand and 4.2:1 for silt.

Equilibrium Bank Slope = 1.76 :1 (H:V) = 0.57 %

Note: The default value of 1.76 is used unless there is information to justify using a different value (different bank material).

#### References

MDOT SHA. 2018. Alternative Headwater Channel and Outfall Crediting Protocol.

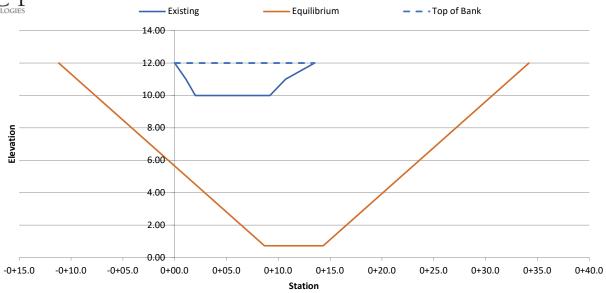
Urban Stormwater Work Group (Stream Restoration Group 2). 2019. Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed. Chesapeake Bay Foundation.

USDA. 2007. Technical Supplement 14B Scour Calculations.

<sup>&</sup>lt;sup>2</sup>Flow depth determined from Manning's equation.



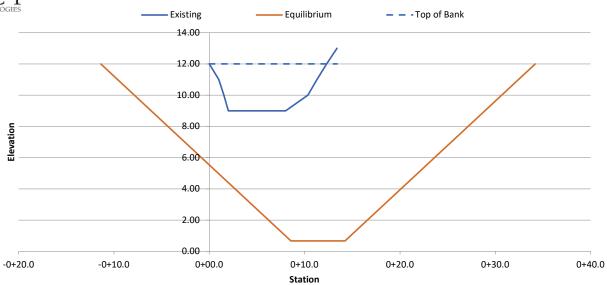
# **Cross Section 1**



BKFL/TOB ELEV=	WIDTH (FT)	WIDTH (FT) MEAN DEPTH (FT)		WIDTH-DEPTH RATIO	DISCHARGE (cfs)
12			(SQ FT)		
EXISTING	13.5	1.5	20.0	9.1	89.2
EQUILIBRIUM	45.4	6.3	287.7	7.2	181.2



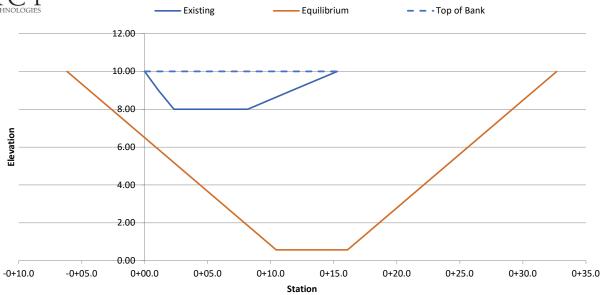
# **Cross Section 2**



BKFL/TOB ELEV= 12	WIDTH (FT)	MEAN DEPTH (FT)	CROSS SECTION AREA (SQ FT)	WIDTH-DEPTH RATIO	DISCHARGE (cfs)
EXISTING	12.3	2.3	28.3	5.4	152.5
EQUILIBRIUM	45.6	6.4	290.4	7.2	230.0



# **Cross Section 3**



BKFL/TOB ELEV= 10	WIDTH (FT)	MEAN DEPTH (FT)	CROSS SECTION AREA (SQ FT)	WIDTH-DEPTH RATIO	DISCHARGE (cfs)
EXISTING	15.3	1.4	21.2	11.0	60.7
EQUILIBRIUM	38.8	5.4	209.8	7.2	153.1

## **Protocol 5 Credit Computations**

Project Name: Harness Creek By: BLE
Project Number: 171804667.16 Check:

# **Nutrient and Sediment Load & Impervious Acre Credit**

Average Bulk Density =  $\frac{93}{\text{Sample TN Concentration}} = \frac{93}{\text{Lb/ft}^3} = \frac{0.047}{\text{tons/ft}^3} = \frac{0.047}{\text{tons/ft}^3} = \frac{0.047}{\text{lb/ton of sediment}} = \frac{1.05}{\text{lb/ton of sediment}} =$ 

Note: For planning purposes, default values of 93 lb/ $\mathrm{ft}^3$  for bulk density and concentrations of 2.28 lb TN/ton of sediment and 1.05 lb TP/ton of sediment may be used.

#### **Potential Sediment:**

	XS 1	XS 2	XS 3	
Cross Section Starting STA =	0	37	77	
Cross Section Ending STA =	37	77	457	
Cross Section Applicable Length =	37	40	380	ft
Existing Channel Cross Sectional Area =	19.96	28.26	21.17	$ft^2$
Equilibrium Channel Cross Sectional Area =	287.73	290.40	209.81	$ft^2$
Volume of Potential Sediment =	9,907	10,486	71,686	$ft^3$

Total Volume of Sediment = 92,079 ft<sup>3</sup>

Total Weight of Sediment = 8,563,332 lb = 4,282 tons

### **Pollutants:**

Removal Efficiency = 56% (50% from Urban Stormwater Work Group, 56% from MDOT SHA)

TN TP TSS

Load = 9,762.20 4,495.75 8,563,332 lbs

Load Reduction = 5,466.83 2,517.62 4,795,466 lbs

Load Reduction Over 30 Years = 182.23 83.92 159,849 lbs/yr

### **Impervious Surface Treatment:**

#### Equation 5. EIAf Calculation for Alternative BMPs

$$EIA_f = \frac{\left(\frac{TN \ Load \ Red.}{I - F_{TN}}\right) + \left(\frac{TP \ Load \ Red.}{I - F_{TP}}\right) + \left(\frac{TSS \ Load \ Red.}{I - F_{TSS}}\right)}{3}$$

Where:

 $EIA_f = Equivalent impervious acre conversion factor$ 

TN Load Red. = BMP load reduction for TN (lbs/unit/yr)

TP Load Red. = BMP load reduction for TP (lbs/unit/yr)

TSS Load Red. = BMP load reduction for TSS (lbs/unit/yr)

 $I - F_{TN} = Aggregate$  impervious unit load minus true forest unit load for TN (lbs/acre/yr)

 $I - F_{TP} = Aggregate$  impervious unit load minus true forest unit load for TP (lbs/acre/yr)

I - F<sub>TSS</sub> = Aggregate impervious unit load minus true forest unit load for TSS (lbs/acre/yr)

#### Table 5. True Forest and Aggregate Impervious Pollutant Unit Load Deltas

ΤN TΡ TSS Aggregate Impervious Unit Load = 20.39 2.55 8,793 lbs/ac/yr True Forest Unit Load = 2.31 0.32 747 lbs/ac/yr Delta = 18.08 2.23 8,046 lbs/ac/yr

 $EIA_f = 22.53$  ac

Length of Channel Requiring Restoration = 457 LF

Acres of Impervious Credit per Linear Foot Restored = 0.05 ac/LF

#### References

MDE. 2020. Accounting for Stormwater Wasteload Allocations and Impervious Acres Treated. Guidance for National Pollutant Discharge Elimination System Stormwater Permits.

Urban Stormwater Work Group (Stream Restoration Group 2). 2019. Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed. Chesapeake Bay Foundation.

# **Appendix E – Stormwater BMP Data Tracking Table**



Heritage Complex 2662 Riva Road Annapolis, MD 21401

Christopher J. Phipps, P.E. Director

# **STORMWATER BMP DATA FORM**

Project Name (List any previous/aka names)	Harness Creek Gully Repair
Contract #	10499
Storm_ID (See Note 5)	
County Project Manager	Melissa Harlinski, PE
Consultant Firm	KCI Technologies, Inc.
Consultant Project Manager	James Tomlinson, PE
BMP Address	600 Quiet Waters Park Rd Annapolis MD, 21403
BMP Location North Easting Coordinates	N 461725; E 1453280
Proposed/Retrofit BMP Type (See note 3)	SPSC
Original/Existing BMP Type (if applicable) (See note 3)	N/A
Proposed/Retrofit BMP Class (See note 4)	RR
BMP Drainage Area (Acres)	12.92
Existing Impervious Area (Acres) to the BMP	1.45
Treated Impervious Area (Acres) to the BMP	2.18
P <sub>e</sub> (provided) (inches)	1.10
Required WQv (ac-ft.)	0.16
Actual WQv (ac-ft.) achieved with Retrofit	0.18
% of the Required WQv captured	109.56%
Retrofit BMP Proposed Date – SD Finalized	N/A
Retrofit BMP Completion Date – CD Finalized	N/A
Length of Shoreline Restored (linear feet)	N/A
Approved % Removal Efficiency for TN	61.0 (Protocol 4), 56.0 (Protocol 5)
Approved % Removal Efficiency for TP	71.4 (Protocol 4), 56.0 (Protocol 5)
Approved % Removal Efficiency for TSS	76.5 (Protocol 4), 56.0 (Protocol 5)
Number of pounds of TN removed	189.11
Number of pounds of TP removed	85.41
Number of tons of TSS removed	162,943
Load Reduction Credit (See note 2)	23.98

#### Notes:

- 1. This form is to be completed and included at the 30% Schematic, Construction design submittal, and as-built stages.
- 2. Use approved EPA CBP Expert Panel Removal Rate methodology. Cite the date and title of the Expert Panel Report used and attaches reference calculations.
- 3. Use MDE BMP Code from the attached
- 4. Use MDE BMP Classification (E, S, or A) from the attached
- 5. Provide the Storm\_Id, if available (For ex. BMP retrofits); If not, use a ID number provided by the County PM. Make sure this ID number is also used on the project plans and reports.
- 6. Provide all associated GIS files for the project per attached "CIP Project GIS Layers Description and Upload Instructions."

Name of professional completing the form	Winnie Boa-Durgammah	Date 04/19/2022
--	----------------------	-----------------

# **Appendix F – Preliminary Cost Estimate**

P584605 Harness Creek Gully Repair 30% Schematic Design Construction Cost Estimate

ITEM	QTY	UNITS	UNIT COST	TOTAL
Mobilization	1	LS	\$25,000.00	\$25,000
Clearing and Grubbing	0.64	AC	\$500.00	\$320
Remove Large Trees	18	EA	\$1,500.00	\$27,000
Maintenance of Traffic	1	LS	\$2,700.00	\$2,700
Orange Safety Fence	1150	LF	\$2.66	\$3,059
Channel or Stream Change Excavation	479	CY	\$16.00	\$7,664
Offsite Disposal of Excess and Unsuitable Materials	234	CY	\$10.00	\$2,344
Maintenance of Stream Flow	1	LS	\$12,000.00	\$12,000
Stablized Construction Entrance	1	EA	\$750.00	\$750
Erosion and Sediment Control Practices	1	LS	\$5,000.00	\$5,000
Cobble	137	CY	\$535.00	\$73,295
Boulders	46	CY	\$250.00	\$11,500
Sand/Woodchip Mix	94	CY	\$123.00	\$11,562
Geotextile Class SE	18	SY	\$10.63	\$191
1" Wood Chips with 3" Compost	138	CY	\$70.00	\$9,660
Natural Fiber Matting	69	SY	\$10.00	\$690
Temporary Stabilization	3092	SY	\$2.50	\$7,730
Landscaping	0.64	AC	\$40,000.00	\$25,600
			Direct Construction Subtotal	\$226,066
			Contingency (30%)	\$67,820
			Construction Subtotal	\$293,886